



# Structural Analysis and Optimization of a Composite Fan Blade for Future Aircraft Engine

*Rula M. Coroneos*  
*Glenn Research Center, Cleveland, Ohio*

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*Rula M. Coroneos*  
*Glenn Research Center, Cleveland, Ohio*

National Aeronautics and  
Space Administration

Glenn Research Center  
Cleveland, Ohio 44135

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Rula M. Coroneos  
National Aeronautics and Space Administration  
Glenn Research Center  
Cleveland, Ohio 44135

## **Abstract**

This report addresses the structural analysis and optimization of a composite fan blade sized for a large aircraft engine. An existing baseline solid metallic fan blade was used as a starting point to develop a hybrid honeycomb sandwich construction with a polymer matrix composite face sheet and honeycomb aluminum core replacing the original baseline solid metallic fan model made of titanium. The focus of this work is to design the sandwich composite blade with the optimum number of plies for the face sheet that will withstand the combined pressure and centrifugal loads while the constraints are satisfied and the baseline aerodynamic and geometric parameters are maintained. To satisfy the requirements, a sandwich construction for the blade is proposed with composite face sheets and a weak core made of honeycomb aluminum material. For aerodynamic considerations, the thickness of the core is optimized whereas the overall blade thickness is held fixed so as to not alter the original airfoil geometry. Weight is taken as the objective function to be minimized by varying the core thickness of the blade within specified upper and lower bounds. Constraints are imposed on radial displacement limitations and ply failure strength. From the optimum design, the minimum number of plies, which will not fail, is back-calculated. The ply lay-up of the blade is adjusted from the calculated number of plies and final structural analysis is performed. Analyses were carried out by utilizing the OpenMDAO Framework, developed at NASA Glenn Research Center combining optimization with structural assessment.

## **1.0 Introduction**

Advanced composites are becoming the material of choice for aircraft engine components. Using composite materials in aircraft engines enables manufacturers to reduce weight, and improve performance. Advanced composite materials are made with either polymer-, metal- or ceramic matrix and high strength fibers. Polymer matrix composites (PMC) are attractive due to their low weight, high strength and low cost for manufacturing complex shaped components. Since 1975, PMCs have been used in jet engines starting with simple components in the fan and bypass duct. A milestone in PMC-technology was set by series production of fan blades for the GE90 engine. Their service temperature however was restricted to a maximum of 150 °C, which is not a limitation for a commercial aircraft engine fan blade. Ceramic matrix composites can withstand much higher temperatures and are thus targeted for use in the hot turbine section of the engine, for parts such as guide vanes, turbine blades and shrouds, to allow increase in-service temperatures and reduce cooling requirements.

Fibrous composite properties are ideal for structural applications such as high-performance aircraft engine blades where high strength-to-weight and stiffness-to-weight ratios are needed. These factors, along with the flexibility to select a composite ply lay-up and fiber orientation to minimize the deformation and the stress under high rotational speeds of future aircraft engines, make a sandwich blade construction attractive.

The objective of this project is to perform structural analysis, design and optimization of a sandwich construction of a given NASA baseline metallic fan blade comparable to a future large aircraft engine fan blade. Polymer matrix composite (PMC) face sheet with aluminum core replaces the metallic blade made of titanium where the fiber material is graphite and the matrix is made from intermediate modulus high strength epoxy-resin. Loads applied include combined centrifugal and pressure. Nonlinear optimization

techniques are used to minimize the overall mass while displacement limitations and ply failure criteria are satisfied. The minimum number of plies for the face sheet is back-calculated using the optimization results. To finalize the task, a final structural analysis is performed to verify the optimized design.

The computer software utilized for analysis and optimization is entitled OpenMDAO (Multi Disciplinary Analysis and Optimization) (Ref. 1) developed at NASA Glenn Research Center (GRC). OpenMDAO is an open-source framework written in Python, providing a number of solvers and optimizers that users can leverage to build their analysis and optimization methods quickly and efficiently. For this project, the structural analysis was performed using MSC/Nastran (Ref. 2) along with two OpenMDAO optimizers NEWSUMT (Ref. 3) and NLPQ (Ref. 4). The content of the report is outlined next.

Description of the baseline finite element model is presented in section 2.0 along with static and dynamic analyses results. In section 3.0, the following topics are described: Formulation of the composite blade design; Grouping of structural elements; Initial ply lay-up configuration; Ply build-up during manufacturing process; Ply failure analysis, and static and dynamic analyses results of the initial composite design. Section 4.0 describes the ply lay-up tailoring using optimization methods, along with the mathematical optimization problem formulation. Optimization results of the composite blade design are presented in section 5.0, including static and dynamic results. Section 6.0 describes the discrete optimization process to obtain the number of plies. Final analysis results and discussion of the optimized composite blade are presented in section 7.0 along with comparison of the initial and final ply lay-up shapes. Final static and dynamic analyses results are also presented in this section. Conclusions are summarized in section 8.0 followed by references.

## **2.0 Description of the Baseline Finite Element Blade**

The baseline finite element model adopted for structural analysis and optimization of a composite design is a NASA fan blade sized for large aircraft engine, as shown in Figure 1. There are 18 fan blades in the metallic baseline design, each with a total mass excluding the hub of 101 lb. The blade span length is 48.5 in., the rotating speed is roughly 1536 rpm, and the design pressure ratio is 1.35 with a bypass ratio of 16.2. A summary of its geometric and aerodynamic parameters is provided below:

Geometric parameters:

Blade span length = 48.5 in.  
Blade tip chord = 28.8 in.  
Blade base chord = 20.07 in.  
Inner radius = 23 in.  
Outer radius = 71.5 in.

Aerodynamic parameters:

Revolutions Per Minute (RPM) = 1536  
Tip speed = 1050 ft/sec  
Leading Edge (L.E.) tip Mach no. = 1.17  
Design pressure ratio = 1.35  
Bypass ratio = 16.2

The material of the baseline solid blades is a titanium alloy, Ti-6Al-4V, with elastic modulus,  $E = 1.60\text{E}+7$  psi, Poisson's ratio,  $\nu = 0.3$ , shear modulus  $G = 6.15\text{E}+6$  psi, mass density,  $\rho = 0.16$  lb/in.<sup>3</sup>, and yield strength =  $1.5\text{E}+5$  psi. The fan tip diameter is 143 in. and the rotation speed is 1536 rpm, rotating about the x-axis. The z-axis is aligned with the blade span axis and the y-axis is perpendicular to the x-z plane. The geometry for one blade is meshed with 9,782 8-nodal hexahedral elements with 15,096 nodes, as shown in Figure 2.

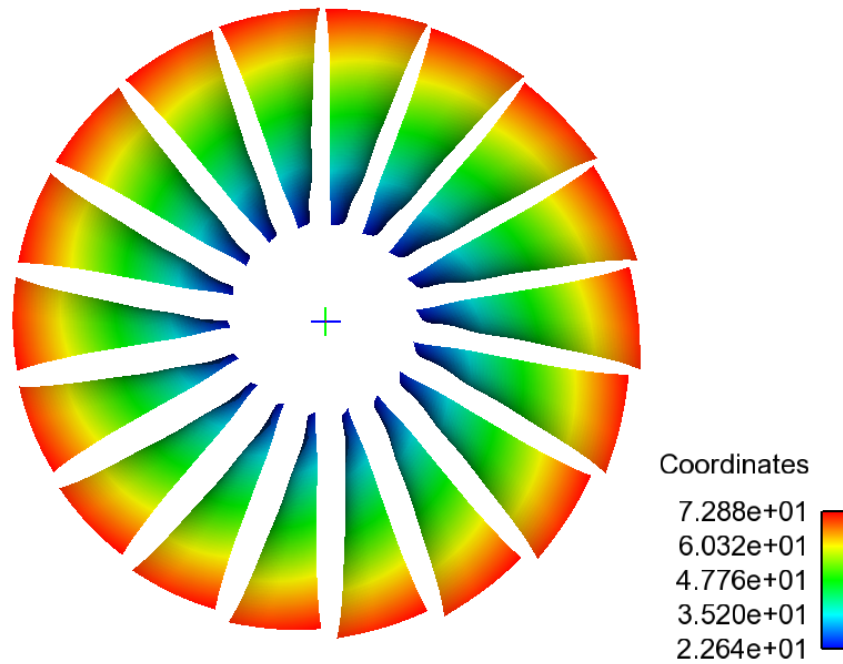


Figure 1.—Baseline model depicting diameter in inches (front view).

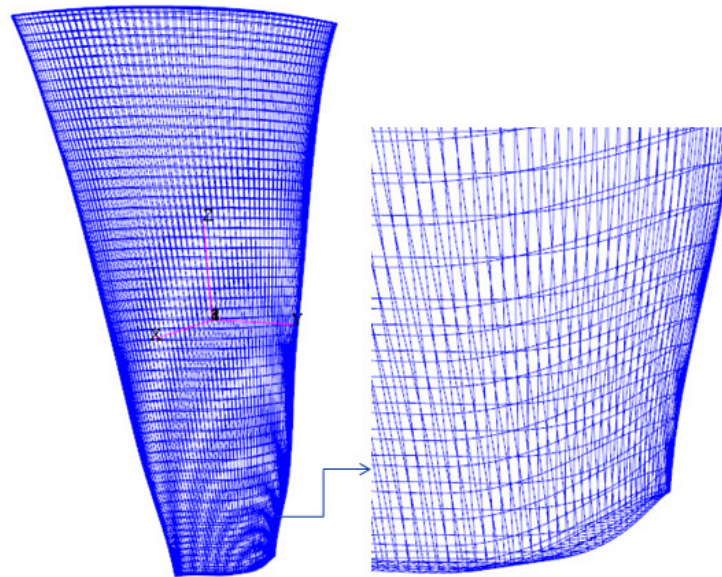


Figure 2.—Finite element model of the baseline fan blade with close up section.

## 2.1 Static Analysis Results of the Baseline Metallic Blade

Due to symmetry of the geometry and the loading, only a single finite element blade model is used in the analysis and optimization of the solid hexahedral model. The blades are acted upon by pressure loads and centrifugal loads. The design pressure ratio is given at 1.35, with a rotational speed of 1,536 rpm along the x-axis. The pressure load, applied on the top surface of the blade, is calculated by subtracting the outflow pressure from the inflow pressure considering 1 atmospheric pressure, 1 ATM = 14.6959 psi:

Outflow pressure =  $1.35 \times 14.6959 = 19.8395$  psi

Inflow pressure = 14.6959 psi

Pressure load = outflow – inflow =  $19.8395 - 14.6959 = 5.1436$  psi

Boundary conditions are fixed on all six degrees of freedom (i.e., rotations and translations) at all nodes at the root of the blade. The blade is analyzed using the MSC/Nastran software, a general purpose finite element solver (Ref. 2). From the MSC/Nastran linear static analysis results, SOL 101, the maximum principal stress is found at node 12 at the root section of the blade at 70,299 psi. The maximum shear stress is at 29,131 psi and the displacement resultant is 4.34 in. at the tip of the blade. The displacement value in z-direction is 0.819 in. The weight of the metallic blade is 100.5 lb. The static analysis results of the baseline metallic blade are summarized in Table 1. Post processing is performed utilizing the MSC/Patran (Ref. 5) software. Plots of the stresses and deformations results are depicted in Figures 3 and 4.

## 2.2 Dynamic Analysis Results of the Baseline Metallic Blade

Dynamic analysis (or modal analysis) of the metallic blade is performed to determine its structural natural frequencies and mode shapes with damping neglected. The natural frequencies of a structure are the frequencies at which the structure naturally tends to vibrate if it is subjected to excitation. The deformed shape of the structure at a specific natural frequency of vibration is termed its normal mode of vibration.

From the theory of vibration the natural frequency  $\omega$  of 1 DOF oscillator is:

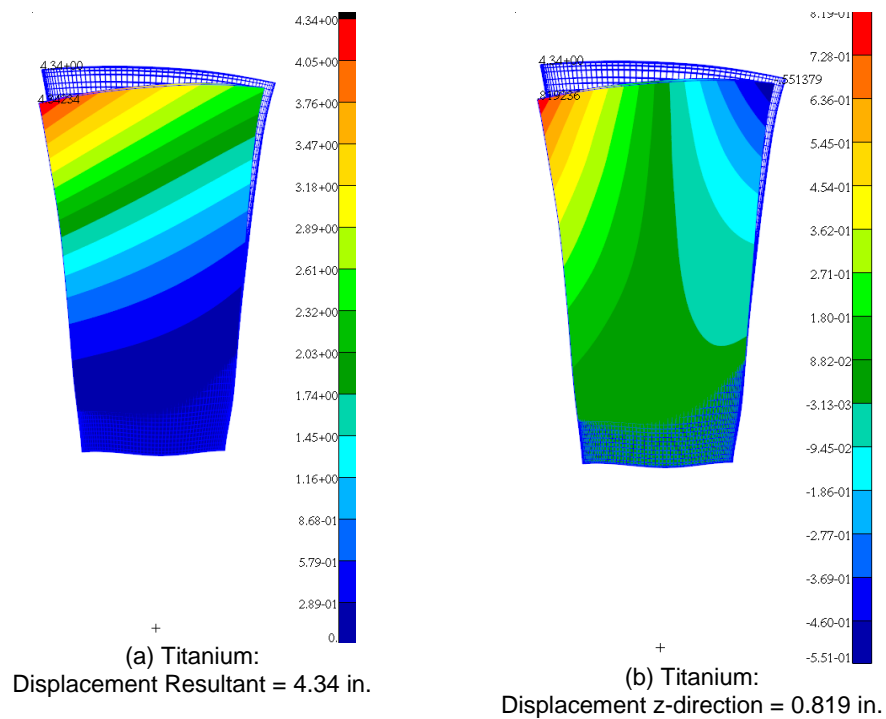
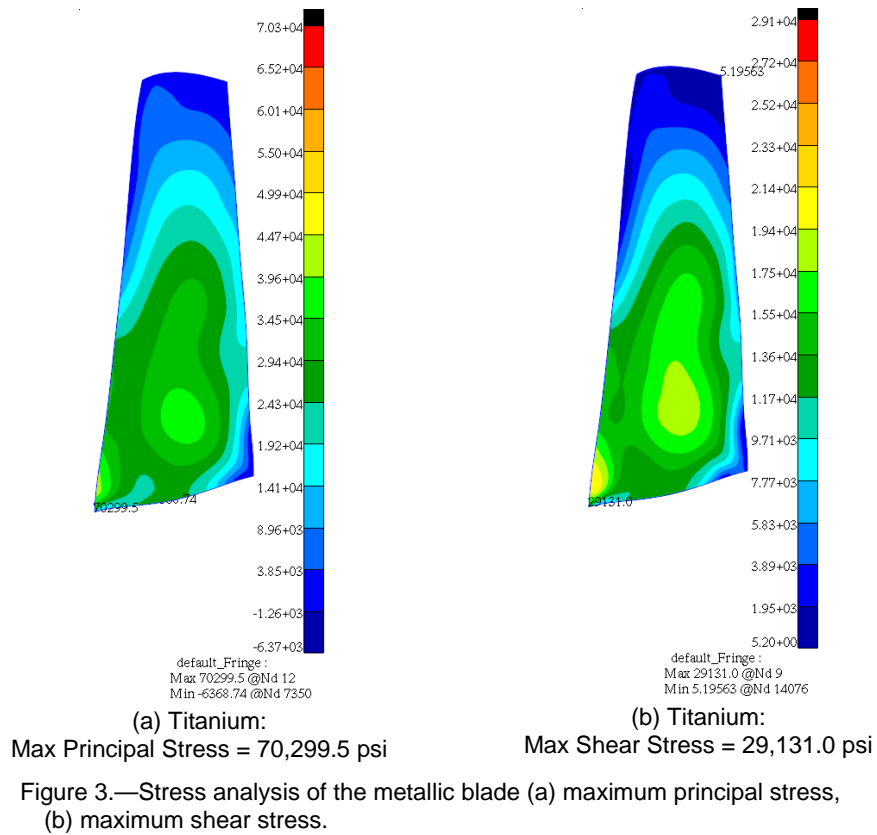
$$\omega = \sqrt{\frac{k}{m}} \quad (1)$$

where  $\omega$  is the radian frequency,  $k$  is the stiffness of the component and  $m$  is the mass. From the radian frequency, the natural frequency in Hertz, (Hz),  $f_n$ , can be found by simply dividing  $\omega$  by  $2\pi$ :

$$f_n = \frac{1}{2\pi} \sqrt{\frac{k}{m}} \quad (2)$$

TABLE 1.—STATIC ANALYSIS RESULTS FOR THE METALLIC BLADE AND CORRESPONDING WEIGHT

Static analysis results	Titanium Alloy Ti-6Al-4V
Max principal stress, psi	70299.5
Max shear stress, psi	29131.0
Displacement, resultant, in.	4.34
Displacement, z-direction, in.	0.819
Weight (lb)	100.528



For the titanium blade:

$$f_n = \frac{1}{2\pi} \sqrt{\frac{1.2625E+4}{1}} = 17.883 \quad (3)$$

where the  $k$  and  $m$  are the calculated generalized stiffness and generalized mass values, respectively.

Results of the first six natural modes from the MSC/Nastran dynamic calculations are summarized in Table 2. All six modes are evenly distributed in the frequency domain. The increment of frequency is 40 to 64 Hz. Fringe plots of the first six natural modes are depicted in Figures 5 and 6. The modes depicted in the figures can be divided into bending modes (1<sup>st</sup>, 2<sup>nd</sup>, 4<sup>th</sup>, and 6<sup>th</sup> modes) and torsion modes (3<sup>rd</sup> and 5<sup>th</sup> modes).

TABLE 2.—NATURAL FREQUENCIES FOR THE METALLIC NASA FAN BLADE

Mode number	Frequency, Hz
Mode 1	17.883
Mode 2	59.339
Mode 3	110.762
Mode 4	151.209
Mode 5	215.544
Mode 6	257.562

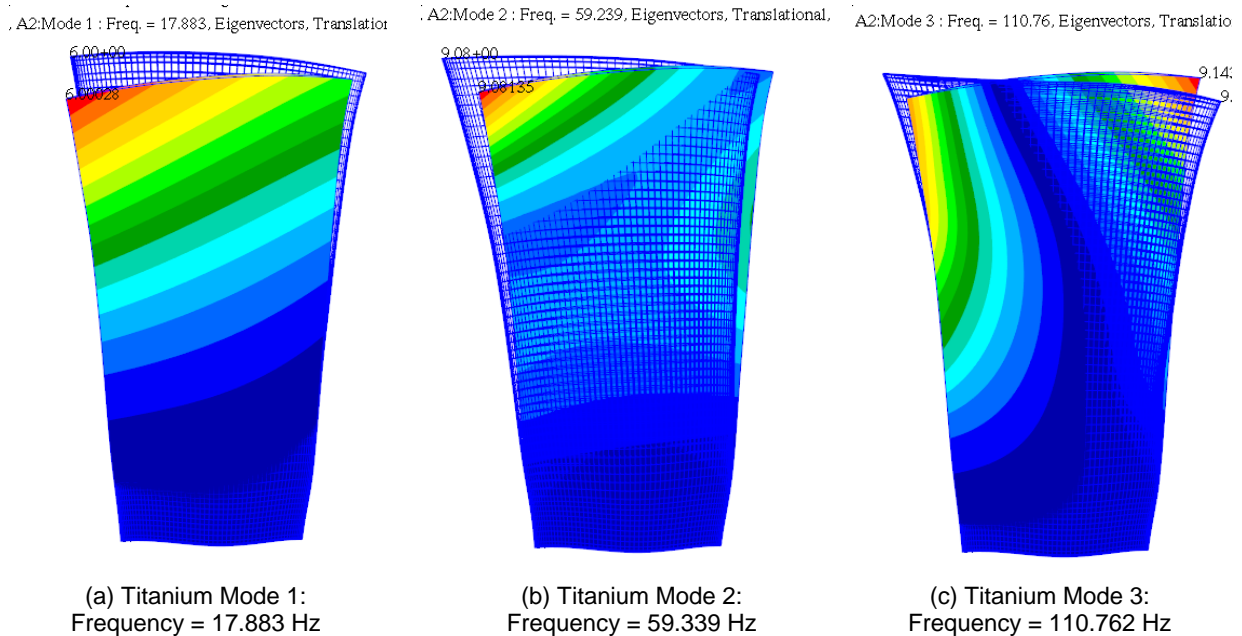


Figure 5.—Mode shapes for the metallic blade: (a) mode 1, (b) mode 2, (c) mode 3.

A2:Mode 4 : Freq. = 151.21, Eigenvectors, Translationa

A2:Mode 5 : Freq. = 215.54, Eigenvectors, Translat

A2:Mode 6 : Freq. = 257.56, Eigenvectors, Translati

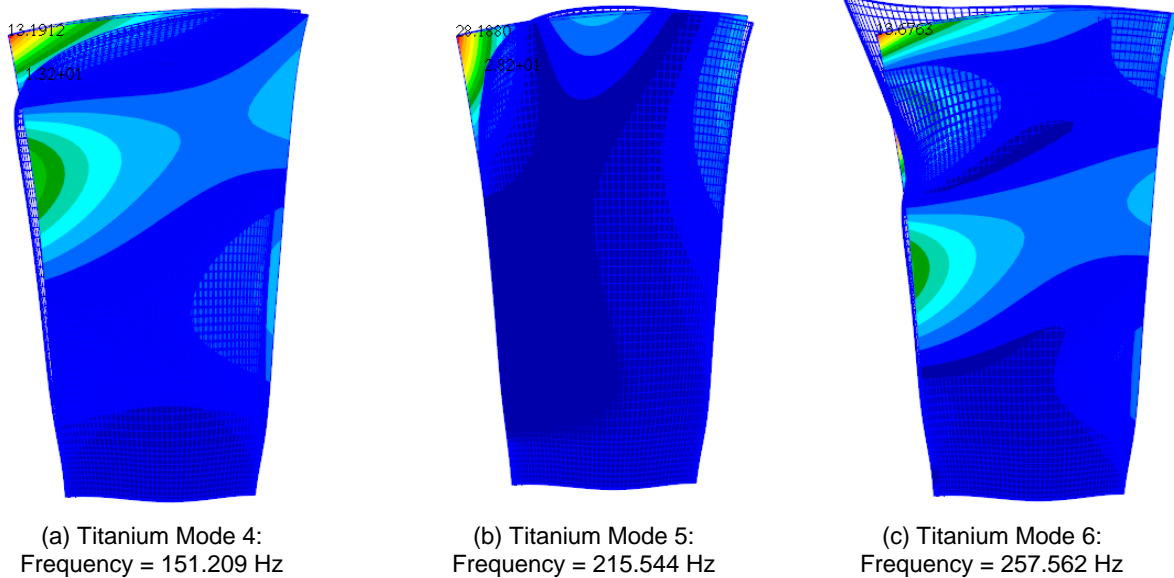


Figure 6.—Mode shapes for the metallic blade: (a) mode 4, (b) mode 5, (c) mode 6.

### 3.0 Formulation of the Composite Blade Design

The baseline solid metallic model was converted into an equivalent two-dimensional shell model and is shown in Figure 7. The conversion to the two-dimensional shell model was required so that the composite laminates could be defined using the layered quadrilateral, CQUAD4 elements with PCOMP (Layered Composite Element Property) in MSC/Nastran (Ref. 2).

The original thickness of each of the elements was maintained by calculating the distance of the coordinate points at the top and bottom surface of the solid model while the middle layer was taken as the face sheet for the two-dimensional shell model. The model conversion was accomplished by using the MSC/Patran (Ref. 5) finite element modeling tool and Fortran programming.

The initial conversion to the two-dimensional quadrilateral mesh created quite a few elements that were out of range, in terms of element aspect ratio and skewness. These elements were all located along the trailing edge and leading edge of the blade as well as at the root and tip of the blade. These caused singularity errors in the static analysis. Therefore, a process was designed to correct the elements and create a new mesh by merging a dozen or more elements at leading and trailing edges including the bottom and top rows at the root and tip of the blade. This process generated a new mesh where the high aspect ratio and skew were eliminated and an aspect ratio of  $<5.0$  was achieved. Merging the elements, rather than eliminating them, ensured that the geometric parameters of the blade remained intact. Figure 7 depicts the updated mesh.

The updated shell model is considered for the sandwich composite ply lay-up design, analysis and optimization. This model consists of 3,162 quadrilateral elements (CQUAD4) and 3,277 nodes, as shown in Figure 7. The blade face sheets are modeled with fiber-reinforced advanced polymer composite materials composed of graphite/epoxy tape fibers and intermediate modulus high strength matrix (Ref. 6). Fixed boundary conditions are applied at the root of the blade in all translations and rotations degrees of freedom. The total remaining number of degrees of freedom are 16,120. Since the geometry and loading of the titanium model is maintained for the composite model, and symmetry is assumed, a single blade is used for the composite analysis and optimization. The same pressure loads and rotation force are imposed upon the blade as the metallic model, i.e., pressure load is 5 psi, and the rotation is 1,536 rpm along the x-axis.

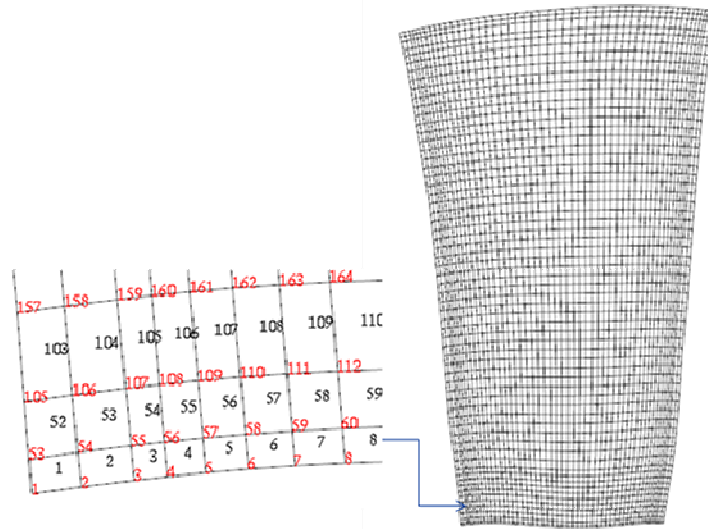


Figure 7.—Finite element model of the equivalent shell model with close-up section (node numbers in red, element numbers in black).

TABLE 3.—POLYMER MATRIX COMPOSITE (PMC) MATERIAL PROPERTIES

Elastic constants	Values	Allowable stresses	Values, psi
Elastic modulus in longitudinal direction, psi (fiber 0° angle)	E11 = 1.94E+7 psi	Allowable tension stress in longitudinal direction Allowable compression stress in longitudinal direction	Xt = 242,500 Xc = 146,904
Elastic modulus in lateral direction, psi (matrix 90° angle)	E22 = 1.19E+6 psi	Allowable tension stress in lateral direction Allowable compression stress in lateral direction	Yt = 13,036 Yc = 30,417
Shear modulus, psi	G12 = 6.32E+5 psi	Allowable stress for in-plane shear	S = 10,940
Poisson ratio	NU12 = 0.26	---	---
Mass density, lb/in. <sup>3</sup>	0.0554	---	---

Unidirectional laminate properties of the graphite/epoxy tape are considered for this model with a fiber volume fraction of 0.6. These are represented using an orthotropic material model for shell elements (MAT8) in MSC/Nastran (Ref. 2). The PMC material properties considered are given in Table 3. The fibers carry most of the applied load. It is important to note that the strength of PMC in the fiber orientation is somewhat greater than the titanium material. On the other hand, the Young's modulus, perpendicular to the fiber orientation, is much smaller.

A sandwich construction for the blade is proposed for this fan blade with composite face sheets and a weak core made of honeycomb material, which is qualified to Boeing BMS 8-124 material specification (Ref. 7). The density of the honeycomb hexagonal cell is small, has weak in-plane stiffness properties and acts as empty space to separate the face sheet and hence, increase the bending stiffness without increasing weight. In addition, it offers significant weight savings, and low manufacturing cost.

Once the material properties have been specified, the next step in the composite analysis is to properly define the fiber orientation. Material property orientation is an important consideration when using composite materials because fiber orientation can greatly influence the deformations since the fibers carry most of the applied load. For the fan blade, the 0° fibers are oriented along the span of the blade (E11), hence the weak orientation is in the transverse direction (E22), perpendicular to the fiber direction. The material orientation is depicted as coordinate axis label 100 in Figure 8.



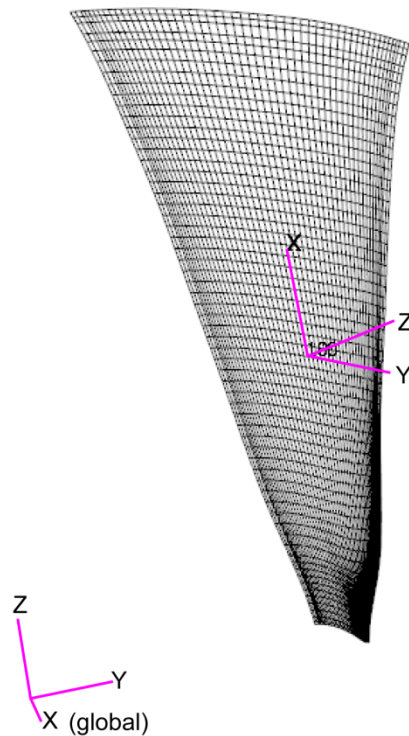


Figure 8.—PMC Material coordinate system (Label 100) with respect to global coordinate system.

### 3.1 Grouping of Structural Elements

When the number of elements in the structure is large, the complexity and computational cost of the overall analysis process increases. For these large structures, the number of design variables is reduced by a technique called design variable linking or element grouping, and is followed for the composite blade. The thickness of each of the elements is essentially the design variable for the optimization. The ply lay-up is also determined from the element grouping and thickness of the elements. The grouping of the 3,162 elements and the thickness of the baseline metallic blade was adopted in formulating the grouping of the CQUAD4 elements and generating the initial design for the composite blade. The grouping process supports and ensures that each group of elements defines a continuous region and that the predefined boundary shapes are retained. Each group of elements references the same property identification number, in the MSC/Nastran analysis.

The blade model was descritized into fifteen groups, which become the design variables (DV) in the optimization problem. The descritization was accomplished by sorting the thickness from thinner to thicker and forming the groups in ascending order. An initial constant ply thickness of 0.025 in. is assumed. The minimum, maximum and average number of plies are based on the thickness of the metallic blade and are calculated as follows:

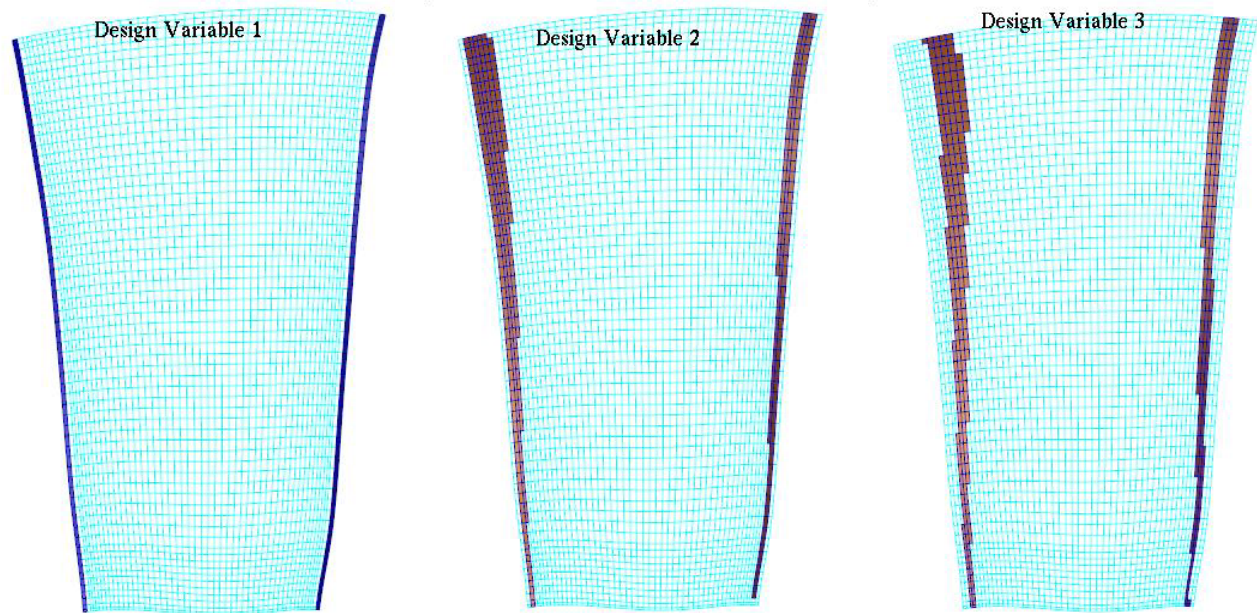
$$\begin{aligned} \text{Min} &= (\text{min\_thickness\_metal}/0.025); \\ \text{Max} &= (\text{max\_thickness\_metal}/0.025); \\ \text{Average number of plies} &= \text{ROUND} (\text{Min}+\text{Max})/2 \end{aligned}$$

The element grouping and number of plies for each design group is depicted in Table 4. As shown in the table, design variable 1 consists of 124 elements, with a thickness range of 0.0596 to 0.09128 in. These elements are on the leading and trailing edges of the blade as shown in dark blue in Figure 9(a). Similarly, design variable 2 consists of 342 elements, with a thickness range of 0.11231 to 0.19979 in. These elements are adjacent to the elements in the previous group, as shown in dark red in Figure 9(b). The individual groups of the elements for design variables 1 to 15 are shown in Table 4 and Figures 9(a) to (c) through Figure 13(a) to (c). The complete assembly of the fan blade element grouping is shown in Figure 14.

The average number of plies was adjusted to accommodate the requirement of a symmetric lay-up, as shown in the last column of Table 4. For aerodynamic considerations, the thickness of the core is varied where as the overall blade thickness is held fixed in order to keep the airfoil geometry and the original model unchanged.

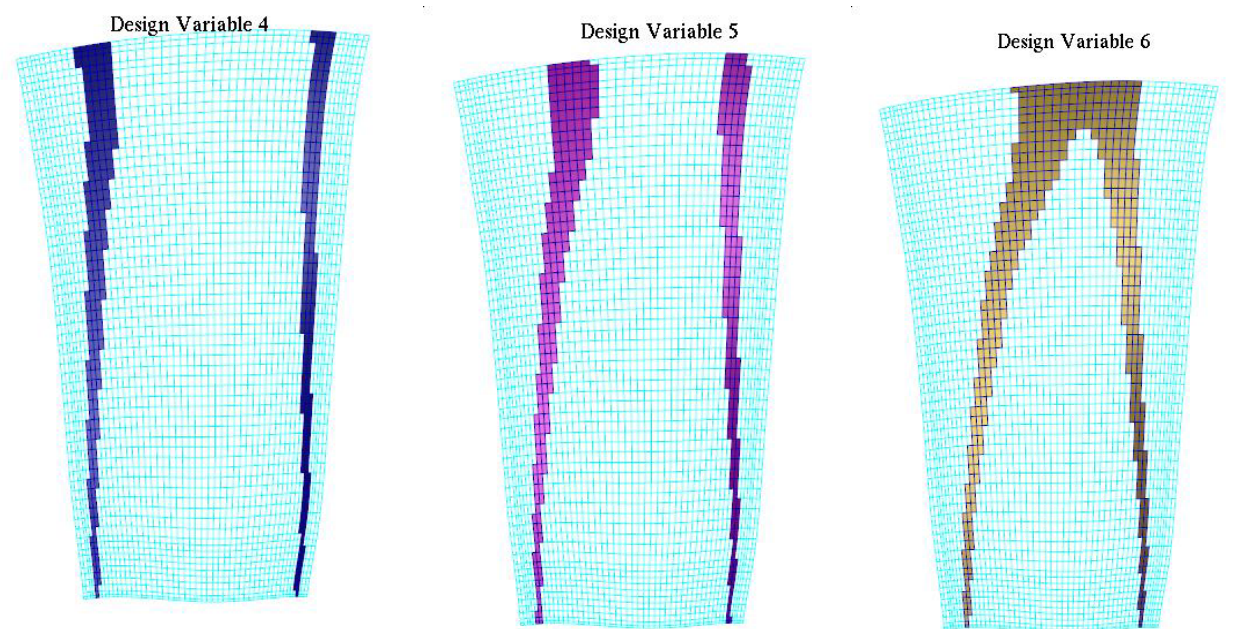
TABLE 4.—ELEMENT GROUPING, THICKNESS RANGE AND NUMBER OF PLIES

Design variable	Number of elements	Thickness range for metal		Number of plies		Average number of plies (rounded)	Adjust for symmetrical laminate
		Min	Max	Min	Max		
1	124	0.0596	0.09128	2.384	3.6512	3	4
2	342	0.11231	0.19979	4.4924	7.9916	6	8
3	363	0.20008	0.29955	8.0032	11.982	10	12
4	334	0.30018	0.39997	12.0072	15.9988	14	16
5	345	0.40057	0.49992	16.0228	19.9968	18	20
6	418	0.50021	0.59996	20.0084	23.9984	22	24
7	333	0.60045	0.69968	24.018	27.9872	26	28
8	241	0.70015	0.79972	28.006	31.9888	30	32
9	173	0.80014	0.89999	32.0056	35.9996	34	36
10	126	0.90032	0.99905	36.0128	39.962	38	40
11	98	1.00013	1.09997	40.0052	43.9988	42	44
12	79	1.1042	1.19811	44.168	47.9244	46	48
13	72	1.20064	1.29819	48.0256	51.9276	50	52
14	62	1.30013	1.39589	52.0052	55.8356	54	56
15	52	1.40059	1.51687	56.0236	60.6748	58	60
Total	3162	---	---	---	---	---	---



(a) DV1: Number of elements = 124      (b) DV2: Number of elements = 342      (c) DV3: Number of elements = 363

Figure 9.—Design variable (DV) groups in dark colors (a) DV1, (b) DV2, (c) DV3.



(a) DV4: Number of elements = 334      (b) DV5: Number of elements = 345      (c) DV6: Number of elements = 418

Figure 10.—Design variable (DV) groups in dark colors (a) DV4, (b) DV5, (c) DV6.



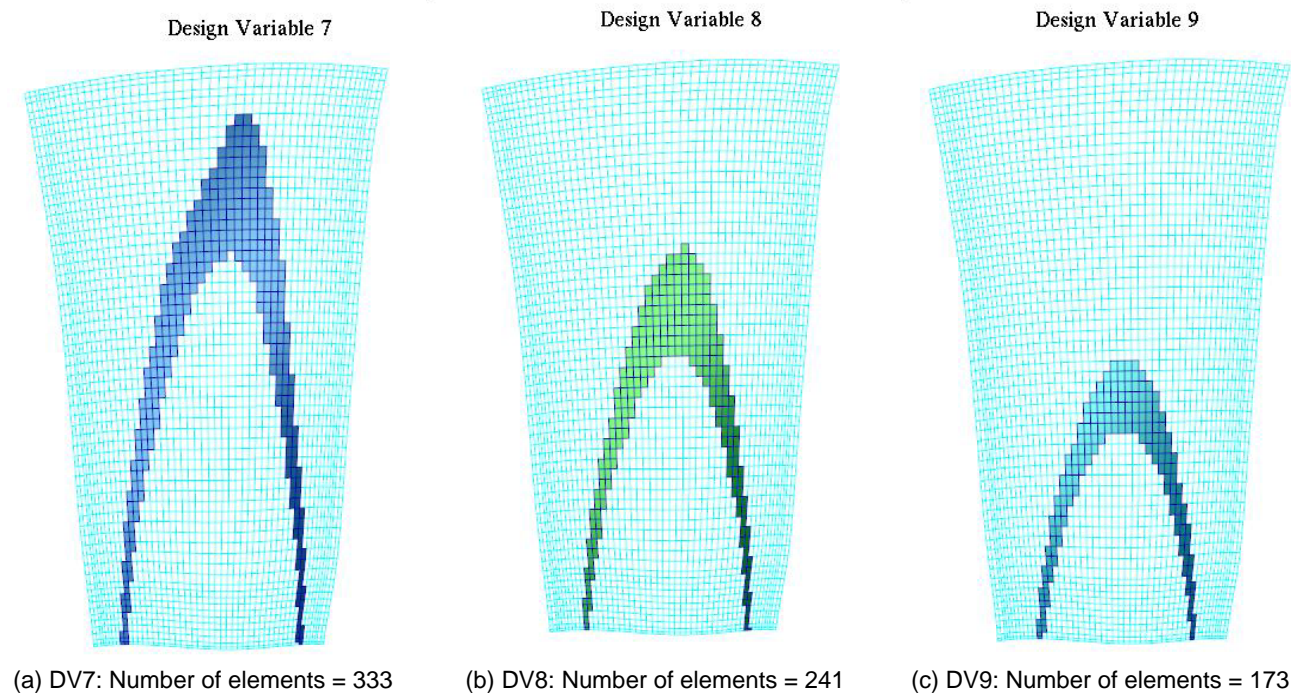


Figure 11.—Design variable (DV) groups in dark colors (a) DV7, (b) DV8, (c) DV9.

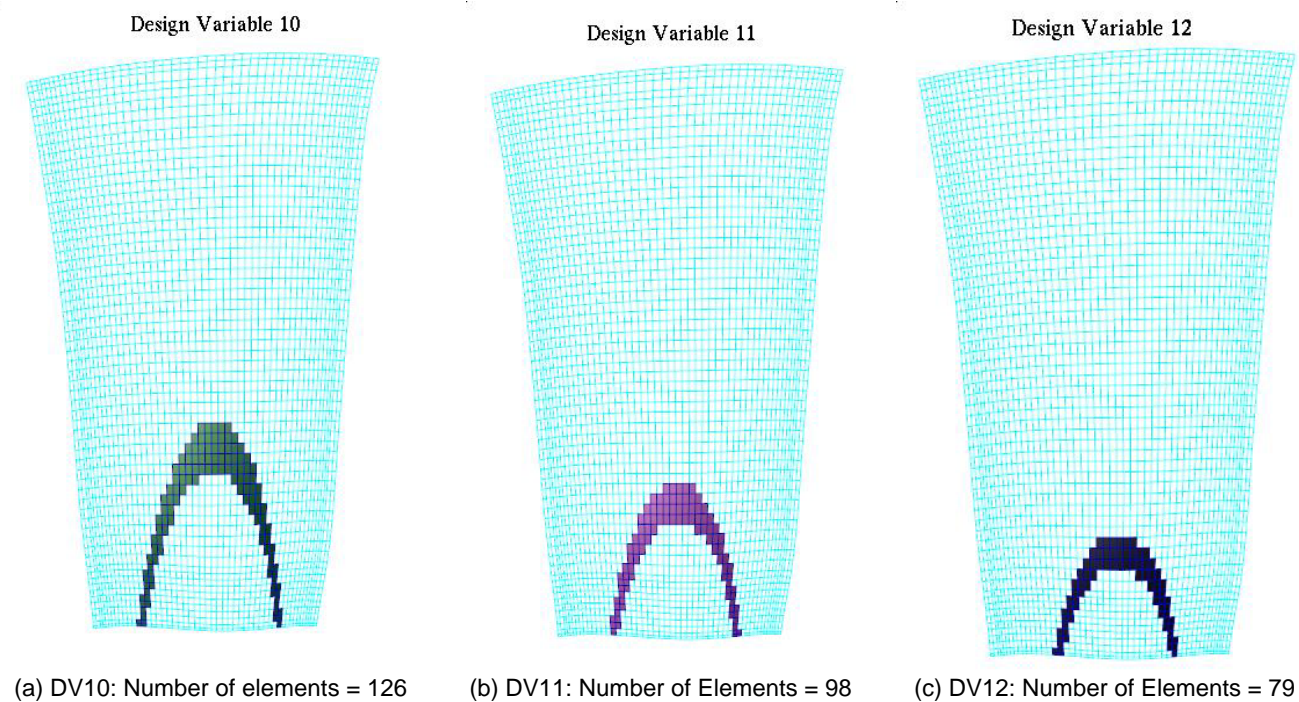


Figure 12.—Design variable (DV) groups in dark colors (a) DV10, (b) DV11, (c) DV12.

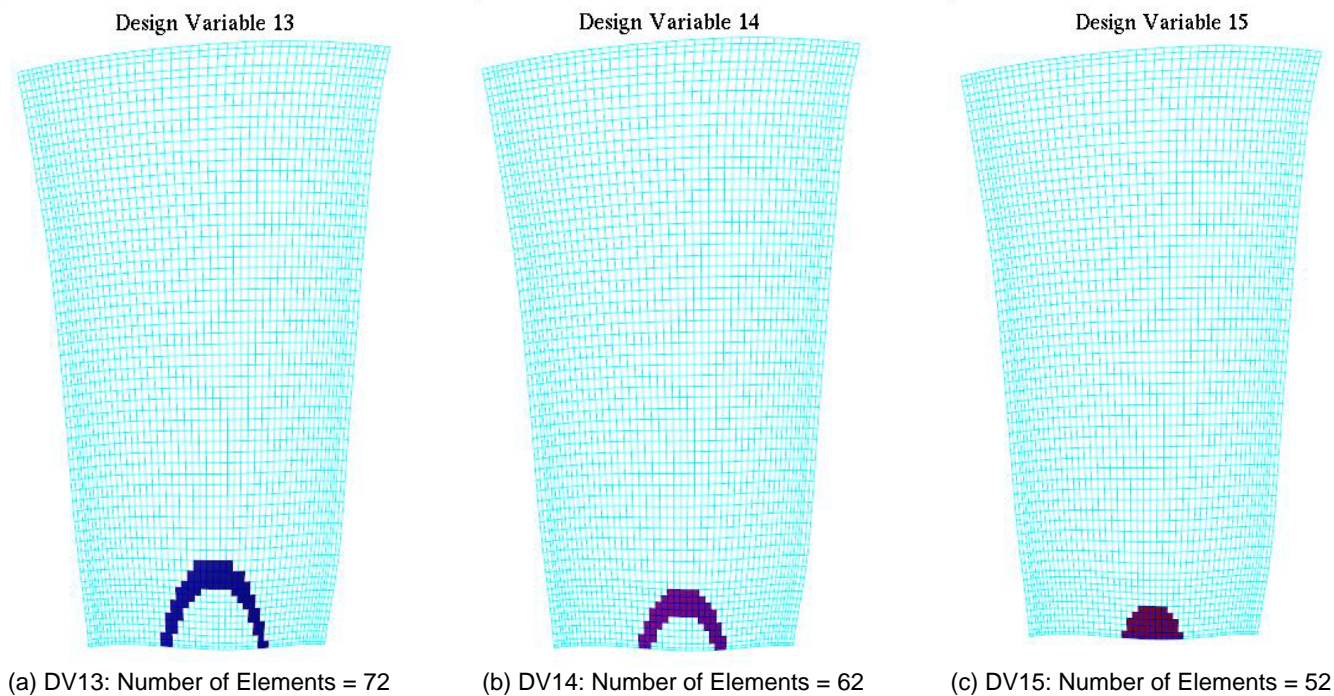


Figure 13.—Design variable (DV) groups in dark colors (a) DV13, (b) DV14, (c) DV15.

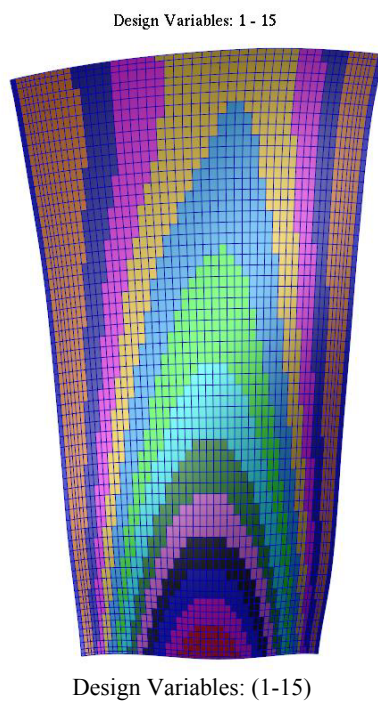


Figure 14.—Complete assembly of design variable groups (1-15).

### 3.2 Initial Ply Lay-Up Configuration

A typical symmetric ply lay-up sequence is assumed at ply orientation angles of  $[0/90/+45/-45]$  degrees. The composite face sheets of group numbers 7 to 15 include the Boeing BMS 8-124 honeycomb material core ply of 0.5 in. thick. The honeycomb core ply is oriented at  $0^\circ$ . The fiber orientations and ply lay-ups were defined on the PCOMP card in MSC/Nastran with an initial thickness of 0.025-in. assuming symmetry. The 'SYM' option is defined on the PCOMP card (Ref. 2) to make the behavior of the laminate symmetric where only plies on one side of the element centerline are specified. The plies are numbered starting with 1 on the bottom layer. Examples of symmetrical laminates are shown in Figure 15.

The composite fan blade initially is designed with about 55 percent of  $[0^\circ/90^\circ]$  plies and 45 percent of  $[\pm 45^\circ]$  plies. The initial ply lay-up for each of the 15 groups is shown in Table 5. The honeycomb core ply of 0.5 in. thick for the composite face sheets, group numbers 7 to 15, defined as 0.25 in. symmetric in the MSC/Nastran PCOMP card, is denoted with an asterisk in Table 5. Initially, the composite fan blade is designed with ten ply lay-up shapes, as shown on the last row of Table 5, and described in the next section.

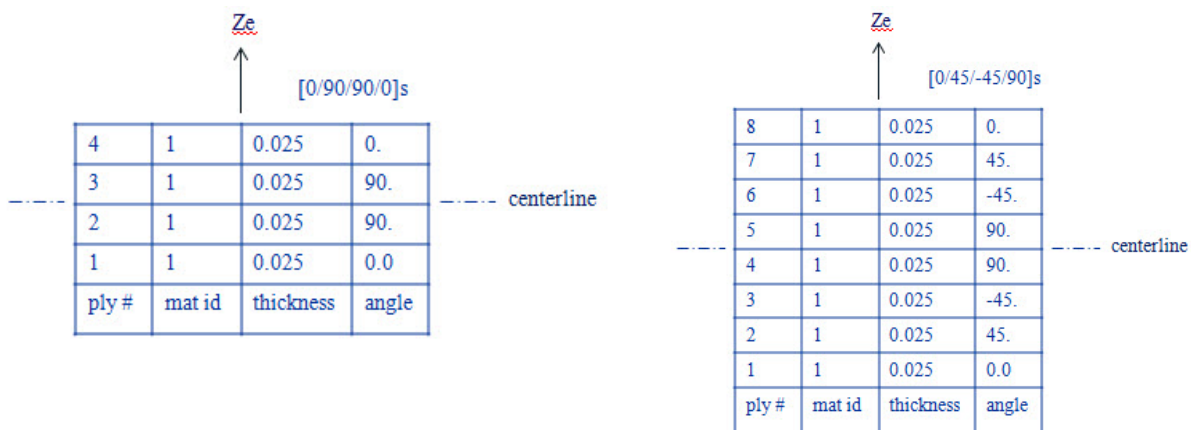


Figure 15.—Ply lay-up in a laminate consisting of symmetrical plies.

TABLE 5.—SYMMETRIC PLY LAY-UP IN THE BLADE LAMINATE, CORE PLY DENOTED WITH AN ASTERISK\*

Group number	Number of plies	Ply angles, Symmetric (S) Ply lay-up
1	4	$[0/90]_s$
2	8	$[0/90/45/-45]_s$
3	12	$[0/90/45/-45/90/0]_s$
4	16	$[0/90/45/-45/90/0/-45/45]_s$
5	20	$[0/90/45/-45/90/0/-45/45/0/90]_s$
6	24	$[0/90/45/-45/90/0/-45/45/0/90/45/-45]_s$
7	8	$[0/90/45/-45/*]_s$
8	12	$[0/90/45/-45/90/0/*]_s$
9	16	$[0/90/45/-45/90/0/-45/45/*]_s$
10	20	$[0/90/45/-45/90/0/-45/45/0/90/*]_s$
11	24	$[0/90/45/-45/90/0/-45/45/0/90/45/-45/*]_s$
12	28	$[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/*]_s$
13	32	$[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/-45/45/*]_s$
14	36	$[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/-45/45/0/90/*]_s$
15	40	$[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/-45/45/0/90/45/-45/*]_s$
Ply Shapes:		1 2 3 4 5 6 7 8 9 10



### 3.3 Ply Build-Up During Manufacturing Process

Advanced composite structures can be manufactured using a wide variety of processes. Each of the fabrication processes has characteristics that define the type of products to be produced. To select the most efficient manufacturing process, the manufacturing team considers several factors such as performance requirements, size of the product, surface complexity, materials, production rate, etc. Common production processes for polymer matrix composites are resin transfer molding (RTM) process and autoclave curing process (Ref. 8). RTM is a low pressure, closed molding process which offers a dimensionally accurate and high quality surface finish composite molding, using liquid thermoset polymers reinforced with various forms of fiber reinforcements. Autoclave curing is typically referring to the process of bonding multiple materials into a single material with the use of an autoclave. Autoclaves are controlled by setting the desired temperature and pressure.

The blade was designed with 15 design groups where each group was specified to have plies oriented at  $[0/90/+45/-45]$  degrees including a honeycomb core ply for design groups (7 to 15). During manufacturing process, the plies are built-up by adding the layers on top of each other. Ten layers or ply shapes in total are required to build the complete blade to form its desired shape, as shown in the last row of Table 5.

The blade is designed initially with a ten ply lay-up shapes or designs as shown in Figures: 16(a) to (c), 17(a) to (c), 18(a) to (c) and Figure 19. For structural integrity, it is very important that some of the plies be continued across the border of the adjacent element groups. Therefore, plies of several element groups share the same orientation. For example, the first ply lay-up shape is made of fibers oriented at  $[0/90]$  degrees, which are stacked together to form the laminate over the entire face sheet of the blade, see Figure 16(a). The second ply shape is made of fibers oriented at  $[+45/-45]$  degrees stacked together to form the laminate over the face sheet of the blade excluding the elements at the edges of the blade having thickness in the range of (0.0596 to 0.09128 in.) or essentially the plies of  $[0/90]$  degrees of element group 1, see Figure 16(b). Similarly, the third ply lay-up shape is made of plies oriented at  $[90/0]$  degrees and is layered over element groups (3 to 6) and (8 to 15), Figure 16(c). The shape of the fourth ply of the lay-up is identified by considering plies oriented at  $[-45/45]$  degrees and covers element groups (4 to 6) and (9 to 15), shown in Figure 17(a). The fifth ply-layup shape is made of plies oriented at  $[0/90]$  degrees of elements groups (5,6) and (10 to 15), see Figure 17(b). The sixth shape is made of fibers oriented at  $[+45/-45]$  degrees and encompasses all elements in groups (6 and 11 to 15), Figure 17(c). The seventh ply lay-up is made of  $[90/0]$  degree plies and encompasses element groups (12 to 15), shown in Figure 18(a). The eighth ply shape lay-up is made of  $[-45/45]$  degree plies and covers element groups (13 to 15), Figure 18(b). The ninth ply lay-up shape is made of fibers oriented at  $[0/90]$  degrees and encompasses element groups 14 and 15, shown in Figure 18(c). The tenth and final ply shape lay-up is made of fiber orientations at  $[45/-45]$  degrees and covers element group 15, shown in Figure 19. The build-up of the honeycomb core ply is also set in place for ply shapes 3 to 10, as shown in Table 5, denoted with an asterisk.

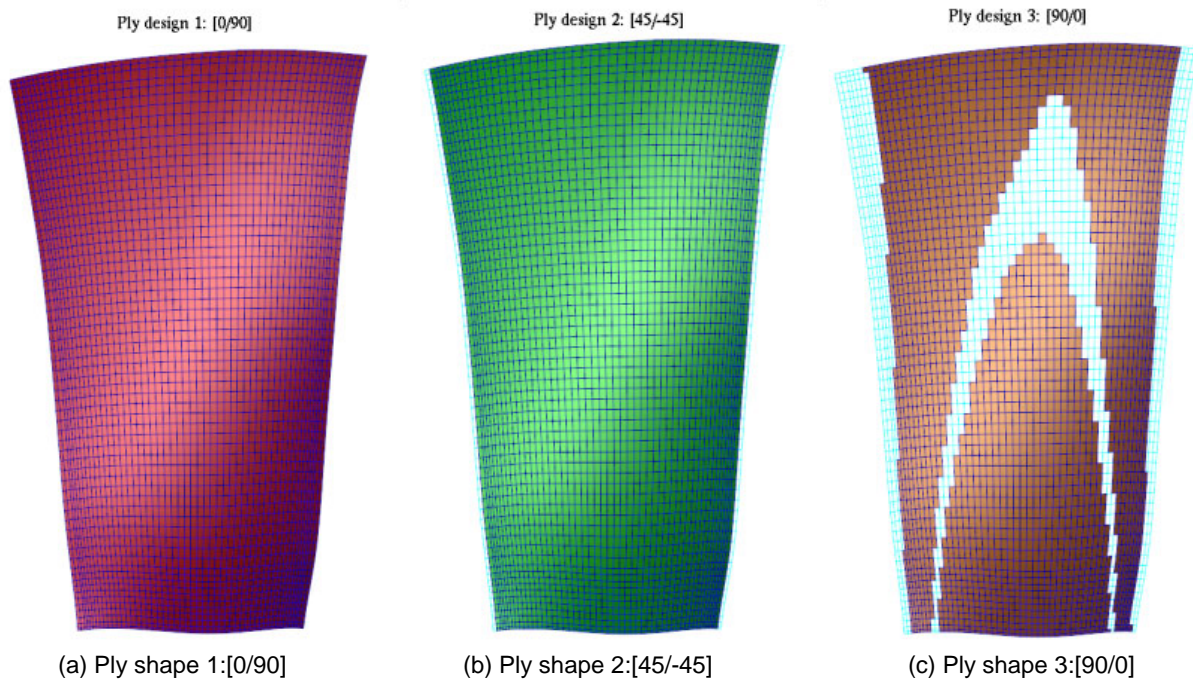


Figure 16.—Ply build-up shapes: (a) shape 1, (b) shape 2, (c) shape 3.

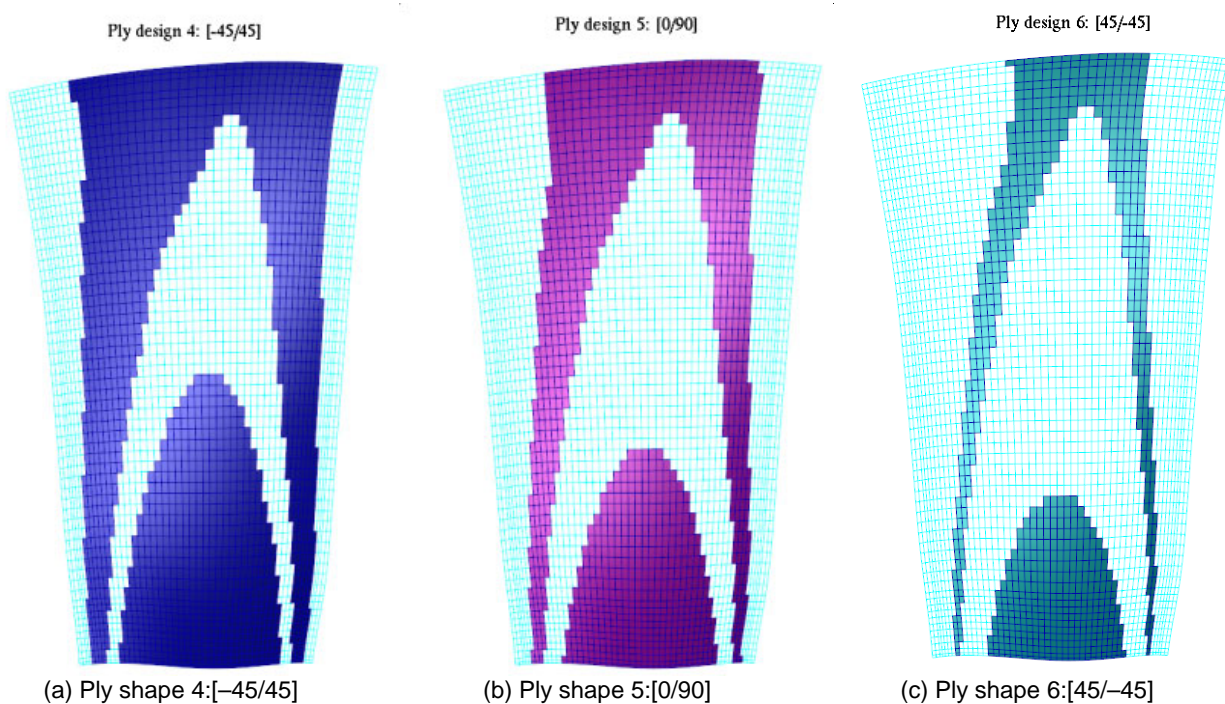


Figure 17.—Ply build-up shapes: (a) shape 4, (b) shape 5, (c) shape 6.



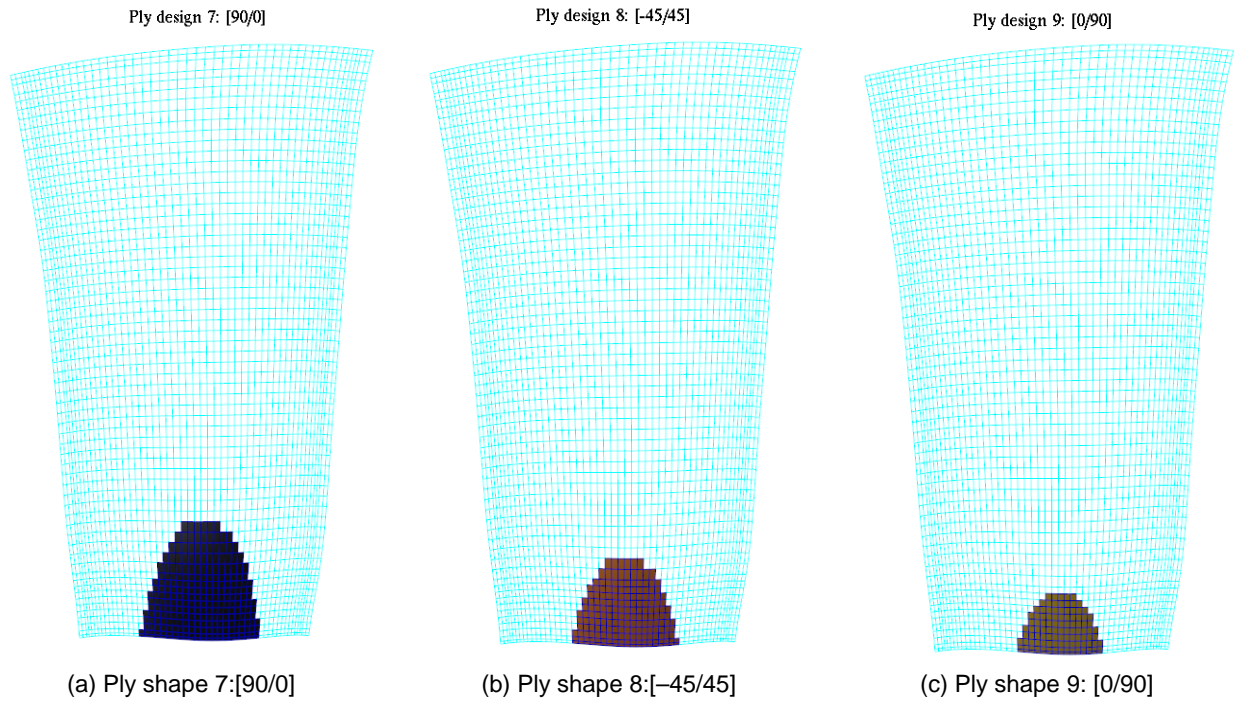


Figure 18.—Ply build-up shapes: (a) shape 7, (b) shape (8), (c) shape 9.

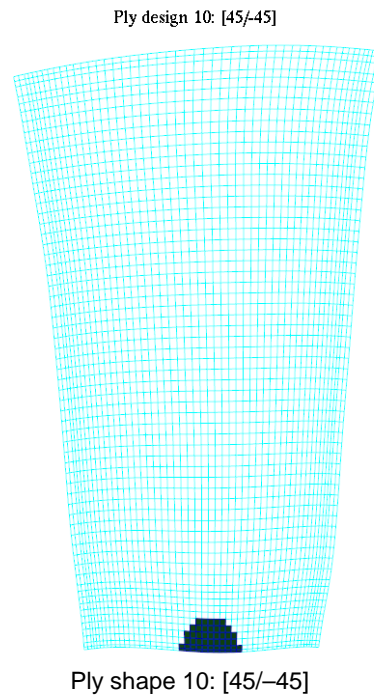


Figure 19.—Ply build-up shape 10.

### 3.4 Ply Failure Analysis

Ply failure analysis is useful to calculate stress failure for any ply lay-up. Ply failure theories have been implemented in MSC/Nastran (Ref. 2) for calculation of residual strength or ultimate load analysis. Failure indices (FI) and strength ratios are used as a linear measure of residual strength. A brief outline on failure index and Strength ratio as implemented in MSC/Nastran is provided next.

#### 3.4.1 Failure Index

Three types of failure theories have been implemented in MSC/Nastran for calculation of failure indices (FI) in the lamina. The theories are: (1) Hill's theory, Hoffman's theory and Tsai-Wu (Tensor Polynomial) theory. Tsai-Wu failure theory is considered for the NASA composite blade analysis, given as:

$$FI = \left( \frac{1}{X_t} - \frac{1}{X_c} \right) \sigma_1 + \left( \frac{1}{Y_t} - \frac{1}{Y_c} \right) \sigma_2 + \frac{\sigma_1^2}{X_t X_c} + \frac{\sigma_2^2}{Y_t Y_c} + 2F_{12} \sigma_1 \sigma_2 + \frac{\tau_{12}^2}{S^2} \quad (4)$$

where  $\sigma_1$ ,  $\sigma_2$ , and  $\tau_{12}$  are the lamina direct and shear stresses along the principal directions and  $X_t$ ,  $X_c$ ,  $Y_t$ ,  $Y_c$  are the allowable tension and compression stresses along principal directions and  $S$  is the allowable shear stress. Typical values for  $F_{12}$  are:

$$F_{12} = \pm 0.5 \sqrt{\frac{1}{X_t X_c Y_t Y_c}} \quad (5)$$

For the composite blade  $F_{12} = 2.43E-12$ . The ply is assumed safe if the value of the failure index is less than 1 and to have failed if the failure index value exceeds 1.

#### 3.4.2 Strength Ratio

First-ply strength ratio (SR) failure concept is implemented in MSC/Nastran (Ref. 2). Strength ratio is a better indicator than failure indices (FI) because it shows how far a ply is to failure and is similar to margin of safety. Failure indices do not show this since they are usually nonlinear functions. For the composite fan blade, the strength ratios are formulated as the constraints in the optimization problem. Strength ratio is calculated in MSC/Nastran using the Tsai-WU failure criteria as follows:

$$\frac{\sigma_1^2}{X_t X_c} + \frac{\sigma_2^2}{Y_t Y_c} + 2F_{12} \sigma_1 \sigma_2 + \frac{\tau_{12}^2}{S^2} + \sigma_1 \left( \frac{1}{X_t} - \frac{1}{X_c} \right) + \sigma_2 \left( \frac{1}{Y_t} - \frac{1}{Y_c} \right) = FI \quad (6)$$

where  $\sigma_1$ ,  $\sigma_2$ ,  $\tau_{12}$  are the actual stresses,  $X_t$ ,  $X_c$ ,  $Y_t$ ,  $Y_c$  are the stress allowable in tension and compression and FI is the failure index, set to 1.0.

Multiplying the actual stresses with the strength ratio (SR) and setting FI = 1.0 the equation becomes:

$$\frac{(SR * \sigma_1)^2}{X_t X_c} + \frac{(SR * \sigma_2)^2}{Y_t Y_c} + 2F_{12} \sigma_1 \sigma_2 (SR)^2 + \frac{\tau_{12}^2 (SR)^2}{S^2} + \sigma_1 SR \left( \frac{1}{X_t} - \frac{1}{X_c} \right) + \sigma_2 SR \left( \frac{1}{Y_t} - \frac{1}{Y_c} \right) = 1.0 \quad (7)$$

Rewriting as:

$$(SR)^2 \left[ \frac{\sigma_1^2}{X_t X_c} + \frac{\sigma_2^2}{Y_t Y_c} + 2F_{12} \sigma_1 \sigma_2 + \frac{\tau_{12}^2}{S^2} \right] + SR \left[ \sigma_1 \left( \frac{1}{X_t} - \frac{1}{X_c} \right) + \sigma_2 \left( \frac{1}{Y_t} - \frac{1}{Y_c} \right) \right] - 1 = 0.0 \quad (8)$$

Solving for the roots (SRs) in the quadratic equation the loads can be linearly scaled based on SR to yield failure index (FI) = 1.0. Strength ratio (SR) of less than 1.0 indicates a failed ply.

### 3.5 Static Analysis Results for the Initial Composite Design

Linear static stress analysis was performed using the finite element software, MSC/Nastran which has been interfaced in the OpenMDAO Framework (Ref. 1). MSC/Patran software is used for pre and post processing of the results (Ref. 5). The intra-lamina ‘Tsai-Wu’ failure criterion is used to find the ply failures. Static analysis results for the initial design of the composite blade are presented in Table 6. The maximum principal stress is at 117,943 psi and the maximum shear stress is at 59,768 psi. Both maximum principal stress and maximum shear stress are higher than the titanium model but they are below their allowable values. The higher stresses are probably due to the reduced thickness of the composite and the inclusion of the honeycomb core. Stress distribution is shown in Figure 20. The displacement magnitude is 9.38 in. with 1.4 in. displacement in the z-direction. The deformed blade shape is shown in Figure 21. For the initial analysis of the composite blade, none of the plies exhibit any failure, since the maximum failure index = 0.6776 or < 1.0 and minimum strength ratio for all plies (SR = 2.38) or greater than 1.0, see Figure 22. The weight savings for the composite blade compared with the titanium model is 75 percent or 25.5 versus 100.5 lb, much lighter as expected.

### 3.6 Dynamic Analysis Results for the Initial Composite Design

Dynamic analysis results for the initial design of the sandwich composite blade were calculated using MSC/Nastran SOL 103 modal analysis solver (Ref. 2). Results of the first six natural modes from the MSC/Nastran dynamic calculations are summarized in Table 7. Similar to titanium results, all six modes are evenly distributed in the frequency domain. Eigenvalue plots of the first six natural modes are depicted in Figures 23(a) to (c) and 24(a) to (c). The modes depicted in the figures can be divided into bending modes (1<sup>st</sup>, 2<sup>nd</sup>, 4<sup>th</sup>, and 6<sup>th</sup> modes) and torsion modes (3<sup>rd</sup> and 5<sup>th</sup> modes).

TABLE 6.—STATIC ANALYSIS RESULTS OF THE INITIAL COMPOSITE DESIGN AND CORRESPONDING WEIGHT

Static analysis results	Composite PMC with honeycomb core
Max principal stress, psi	117943.0
Max shear stress, psi	59768.47
Displacement, resultant, in.	9.38
Displacement, z-direction, in.	1.40
Weight (lb)	25.557

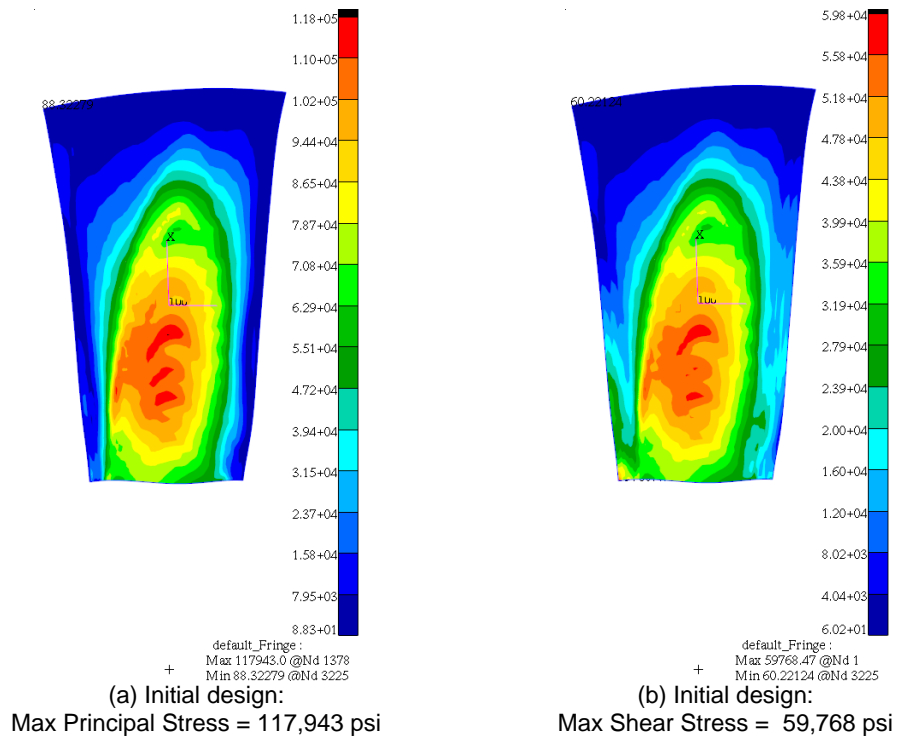


Figure 20.—Stress distribution results for the composite initial design (a) maximum principal stress, (b) maximum shear stress.

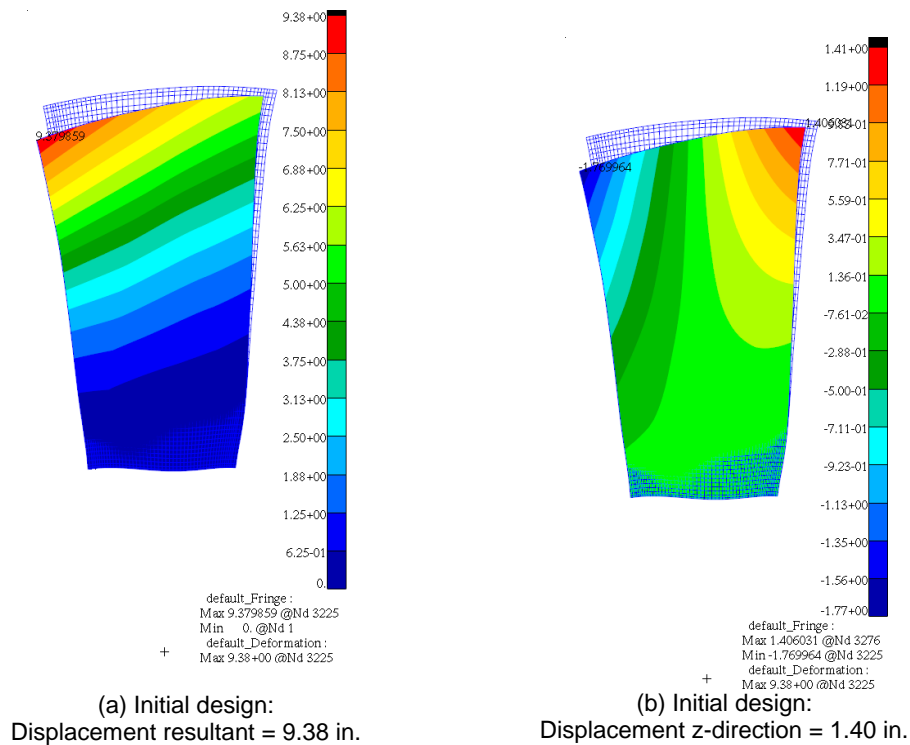


Figure 21.—Deformation results for the composite initial design (a) displacement resultant, (b) displacement in z-direction.

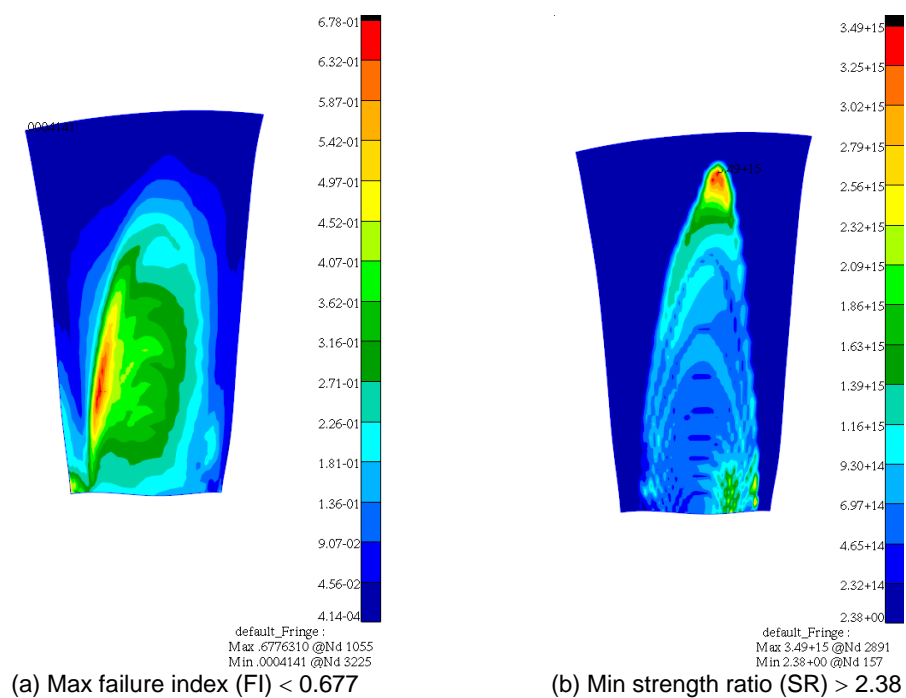


Figure 22.—Ply failure analysis results for the composite initial design (a) failure index, (b) and strength ratio.

TABLE 7.—NATURAL FREQUENCIES FOR THE INITIAL COMPOSITE DESIGN

Mode number	Frequency, Hz
Mode 1	19.473
Mode 2	58.792
Mode 3	110.320
Mode 4	150.936
Mode 5	248.470
Mode 6	263.912

:DEFAULT, A1:Mode 1 : Freq. = 19.473, Eigenvectors, 'DEFAULT, A1:Mode 2 : Freq. = 58.792, Eigenvectors, 'DEFAULT, A1:Mode 3 : Freq. = 110.32, Eigenvectors, '

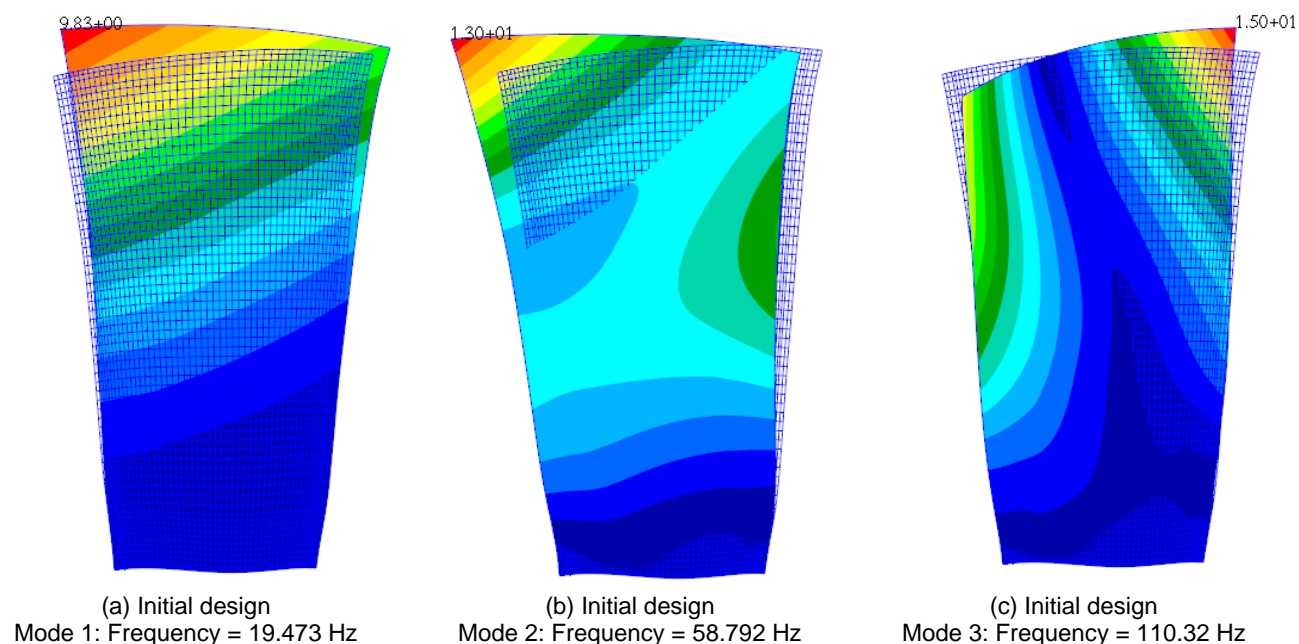


Figure 23.—Fringe plots of mode shapes for the composite initial design (a) mode 1, (b) mode 2, (c) mode 3.

:DEFAULT, A1:Mode 4 : Freq. = 150.94, Eigenvectors, 'DEFAULT, A1:Mode 5 : Freq. = 248.47, Eigenvectors, TraDEFAULT, A1:Mode 6 : Freq. = 263.91, Eigenvectors, '

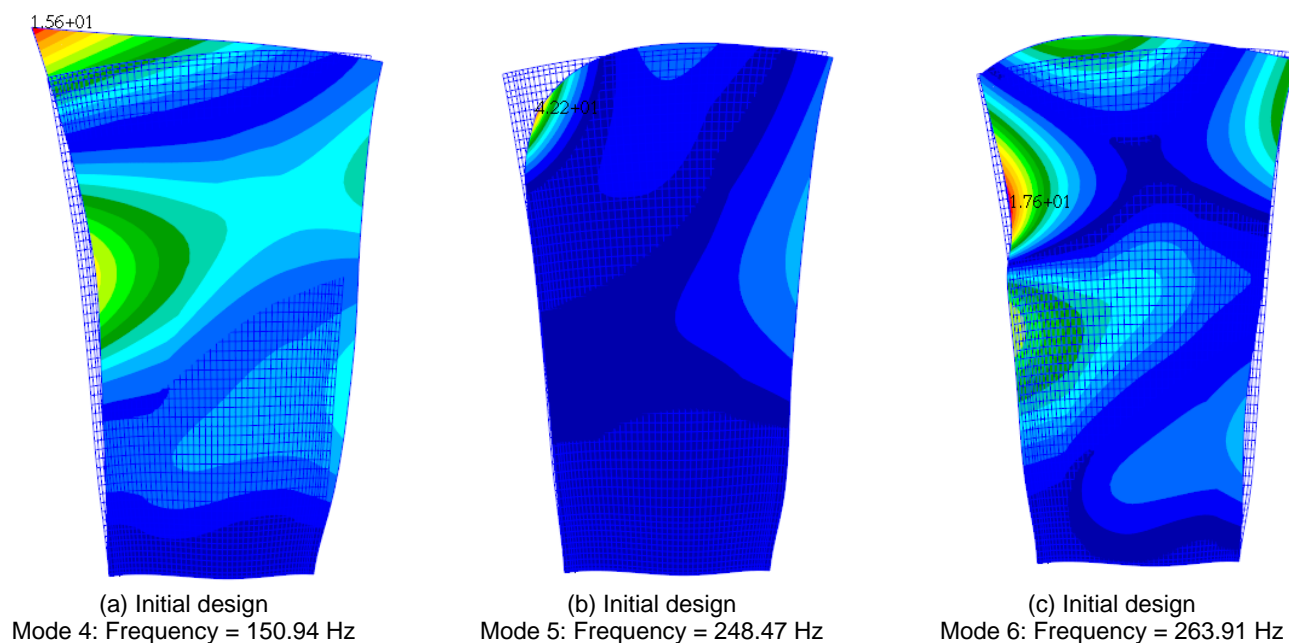


Figure 24.—Fringe plots of mode shapes for the composite initial design (a) mode 4, (b) mode 5, (c) mode 6.

## 4.0 Ply Lay-Up Tailoring Using Optimization Methods

This step in composite optimization process is to make use of the methods of nonlinear programming to solve the optimization problem utilizing the design concepts of the composite structure while the constraints imposed on radial displacement limitations and ply failure strength ratio criteria are satisfied and the baseline aerodynamic and geometric parameters are maintained.

Weight reduction is taken as the objective function by varying the core thicknesses of the blade within specified upper and lower bounds as the design variables. Constraints are imposed on radial displacements limitation at the two tip nodes and at the same time the strength ratio of the plies is constrained within the allowable range, following the MSC/Nastran “first-ply” strength ratio failure concept. Details of the optimization formulation is provided next.

### 4.1 Mathematical Optimization Problem Formulation

The formal expression for the structural optimization of a sandwich composite laminate shell or plate structure is:

$$\text{Minimize } W(x) \quad (9)$$

Subject to stress and displacement constraints:

$$g_j(x) \leq 0, \quad j = 1, \dots, N_s + N_d \quad (10)$$

where  $W$  represents the weight,  $g$  denotes the constraints,  $N_s$  represents the number of stress constraints,  $N_d$  represents the number of displacement constraints and  $x$  represents the independent active design variables within prescribed lower ( $LB$ ) and upper bounds ( $UB$ ) as:

$$(x_i^{LB} \leq x_i \leq x_i^{UB}, i = 1, 2, \dots, n) \quad (11)$$

where  $n$  is the total number of design variables. The nonlinear programming optimization formulation of the composite blade is as follows:

#### 4.1.1 Objective Function

The objective function is to minimize the weight of the blade given by:

$$W = \sum_{j=1}^m \rho_j A_j t_j \quad (12)$$

where  $\rho_j$  is the material density for each member,  $A_j$  is the cross-sectional area of the shell element,  $t_j$  is the thickness of the element and  $m$  is the total number of elements, or 3162 elements.

#### 4.1.2 Constraints

For the blade, the constraints  $g$ , are imposed on the strength ratio for each ply group as well as radial displacements on two tip nodes. The two tip nodes are shown in Figure 25. The calculation of the strength ratio depends on the evaluated stress and is implemented in MSC/Nastran using the TSAI-WU failure criteria, given in Equation (8). The strength ratio can be considered as margin of safety and shows how far along the particular ply is to failure.

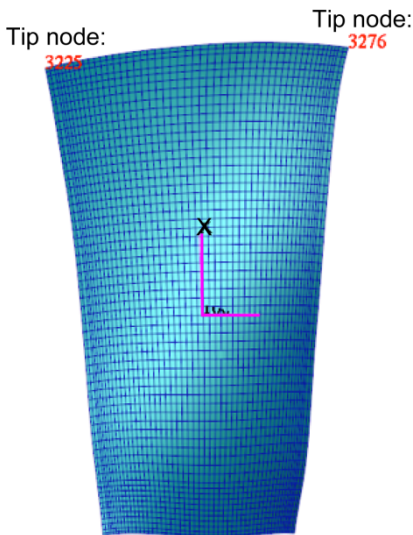


Figure 25.—Node number locations of radial displacements.

#### 4.1.2.1 Strength Ratio Constraints

For the composite blade optimization, the strength ratio constraints are formulated as:

$$g_j = 1 - \frac{SR_j}{SR_0} \leq 0, \quad j = 1, \dots, Ns \quad (13)$$

where  $SR_j$  is the strength ratio parameter calculated as the ratio between failure stress and the actual stress,  $SR_0$  is the safety factor and  $Ns$  is the number of stress constraints. For the blade, the strength ratio for the 15 design groups are considered as the constraints in the optimization problem. The limitation on the strength ratio includes a safety factor (SF) in the range of ( $1.5 < SF < 3.0$ ). The strength ratio constraints taking into account the safety factor are formulated as:

$$g_j = 1.5 - \frac{SR_j}{SR_0} \leq 0, \quad j = 1, \dots, 15 \quad (14)$$

$$g_j = \frac{SR_j}{SR_0} - 3 \leq 0, \quad j = 1, \dots, 15 \quad (15)$$

#### 4.1.2.2 Radial Displacement Constraints

The equation which describes the radial displacement at any radial position is the dot product of the displacement vector and the unit vector in the radial direction, given as:

$$v_R = \frac{r \cdot u}{|u|} \quad (16)$$



where  $r$  is the displacement value obtained from static analysis in y-z plane at the tip node and  $u$  is the (y, z) coordinate locations of the tip node. For the blade, x-axis is the axis of rotation and consequently when y and z are zero we are at the center of the circle. Therefore, the y and z coordinates of a given point also represents the radial direction. The displacement constraints in the optimization computer code are specified as:

$$g_j = \frac{u}{u_0} - 1 \leq 0, \quad j = 1, 2 \quad (17)$$

where  $u$  is the calculated radial displacement at the tip of the blade,  $u_0$  is the maximum displacement allowable or 0.5 in., taking into consideration the deformed blade tip clearance requirement of less than or equal to 0.5 in. The total number of displacement constraints is 2. For the composite blade, the two radial displacements are calculated at the corner tip nodes, 3225 and 3276 of the leading and trailing edges, as shown in Figure 25.

Coordinate locations and displacement values at tip node 3225 are expressed as:

$$u = \begin{Bmatrix} y \\ z \end{Bmatrix} = \begin{Bmatrix} -12.1351 \\ 71.3424 \end{Bmatrix}; \quad r = \begin{Bmatrix} -7.9256 \\ -1.7210 \end{Bmatrix} \quad (18)$$

where vector  $u$  represents the coordinates values and  $r$  the displacement values from the static analysis run. The radial displacement at tip node 3225 is calculated as follows:

$$v_R = \frac{r \cdot u}{|u|} = \frac{(-7.9256)(-12.1351) + (-1.7210)(71.3424)}{\sqrt{(12.1351)^2 + (71.3424)^2}} = \frac{-26.6023}{72.3671} = -0.3676 \text{ in.} \quad (19)$$

Coordinate locations and displacement values at tip node 3276 are:

$$u = \begin{Bmatrix} y \\ z \end{Bmatrix} = \begin{Bmatrix} 10.3786 \\ 69.7165 \end{Bmatrix}; \quad r = \begin{Bmatrix} -5.6709 \\ 1.3826 \end{Bmatrix} \quad (20)$$

where  $u$  represents the coordinates values and  $r$  the displacement values from the static analysis run. Radial displacement at tip node 3276 is calculated via the expression:

$$v_R = \frac{r \cdot u}{|u|} = \frac{(-5.6709)(10.3786) + (1.3826)(69.7165)}{\sqrt{(10.3786)^2 + (69.7165)^2}} = \frac{37.534}{70.4848} = 0.5325 \text{ in.} \quad (21)$$

#### 4.1.3 Design Variables

Fifteen design variables are specified in the formulation of the sandwich composite blade. These design variables represent the linking of the 3162 elements into the 15 ply groups. Design variables are defined such that by selecting an initial ply thickness and allowing the thickness of the core plies to vary with a particular fiber orientation for every element, the total laminate thickness can change continuously throughout the blade and at the same time, the shape of the aerodynamic profile remains fixed. Since the honeycomb core ply is constructed for design variables 7 to 15, the first 6 design variables are considered

passive in the optimization process. Manufacturing constraints or side constraints such as lower and upper bounds on the plies are imposed, limiting the size of the core thickness variables as:

$$(x_i^{LB} \leq x_i \leq x_i^{UB}, i = 1, 2, \dots, n) \quad (22)$$

where  $x$  represents the design variable,  $LB$  and  $UB$  are the lower and upper bounds respectively and  $n$  is the number of design variables.

In the optimization process, the general formula to update the design variables,  $(x_j)$  in a nonlinear programming algorithm at the  $k^{\text{th}}$  intermediate iteration is given as:

$$\{x\}_k = \{x\}_{k-1} + \alpha_{k-1} \{d\}_{k-1} \quad (23)$$

where the step length  $\alpha_{k-1}$  is calculated to find the local minimum of the objective or weight in this study along the direction  $\{d\}_{k-1}$  in the feasible domain.

## 5.0 Optimization Results of the Composite Blade Design

Optimization algorithms NEWSUMT (Ref. 3) and NLPQ (Ref. 4), both available in OpenMDAO Framework (Ref. 1), are used for obtaining the optimum design of the composite sandwich fan blade.

The minimization algorithm used in NEWSUMT is a Sequence of Unconstrained Minimizations Technique. The major features of NEWSUMT include a modified Newton's method where the second derivatives of the penalty function are approximated by expressions involving only the first derivatives. Another major feature is an extended interior penalty function formulation where it combines the interior and exterior penalty functions. The code is written in Fortran and is very efficient for solving linear and nonlinear constrained or unconstrained minimization problems. This optimizer is included in the OpenMDAO standard library to provide users with a basic gradient-based optimization algorithm.

NLPQ is another gradient-based optimizer available in OpenMDAO although, it is not publicly accessible. NLPQ (NonLinear Programming by Quadratic Lagrangian) solves nonlinear optimization problems. NLPQ generates a sequence of quadratic programming subproblems obtained by a quadratic approximation of the Lagrangian function and linearization of constraints. This algorithm is also very efficient and in most cases requires fewer function calls than NEWSUMT. However, this algorithm has recently been implemented in the OpenMDAO Framework and the default parameters, such as convergence criteria and step length have been used in the present work, thus requiring greater CPU time than NEWSUMT method. Further development of the OpenMDAO is expected to result in significantly shorter CPU time for the NLPQ optimizer.

In general, structural optimization takes a great deal of computation time because in every iteration a complete finite element analysis is required. The number of iterations, however, can be kept down by a good estimate of the initial values of the design variables. On the other hand, for the sandwich composite blade model, it is nearly impossible to predict a favorable initial design for each layer because of the complexity of the fan blade design and the ply lay-up shapes.

The CPU time in the optimization process for the composite blade design running on a Linux x86\_64 workstation at 2.67 GHz was high. NEWSUMT optimizer took 79,799 sec or 22 hr and NLPQ 95,820 sec or 26 hr.

### 5.1 Static Results of the Optimized Composite Design

The optimum weight iteration history plot obtained from the two optimization methods is shown in Figure 26. It should be noted that the initial design was not feasible because at least one strength ratio

constraint was violated, in particular constraint numbers 1, 7, and 8, as shown in Table 10. The optimum weight calculated by NEWSUMT was 27.68 lb. The CPU time to convergence was 22 hr with 34 iterations, 998 objective function calls, 408 constraint functions and 284 approximate constraint function calls. The weight is slightly higher than the initial weight of 25.56, but this is reasonable as explained in the next section observing the activity of the response constraints. The convergence from NLPQ optimizer was not achieved at the maximum number of iterations allowed, 100, although the CPU time for NLPQ was 26 hr. Figure 26 shows that the optimizer had reached convergence at about iteration number 60, but due to some other parameter setting, was not able to stop. The weight by NLPQ is 28.07 lb, which is also slightly higher than the initial weight of 25.56 lb by 9.75 percent, as shown in Table 8.

Maximum principal stress and maximum shear stress results with percent differences are given in Table 8. Principal stress values were reduced from the initial design by about 8 percent for both optimization methods. Shear stresses were also reduced by both methods by about 9.5 percent. The magnitude of the displacement was reduced by about 8.8 percent for both NEWSUMT and NLPQ optimizers. Deformation results are depicted in Table 9.

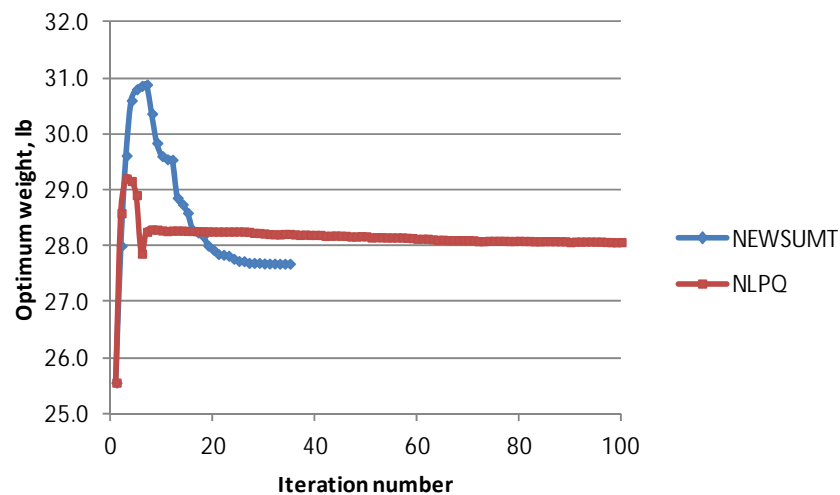


Figure 26.—Optimum weight with number of iterations from NEWSUMT and NLPQ.

TABLE 8.—COMPARISON OF STATIC ANALYSIS RESULTS AND WEIGHT FOR INITIAL AND OPTIMUM DESIGNS

	Initial	NEWSUMT optimum	NLPQ optimum	Percent difference NEWSUMT	Percent difference NLPQ
Max principal stress, psi	117943.0	108102.0	107921.2	−8.34	−8.50
Max shear stress, psi	59768.47	54051.13	53960.69	−9.57	−9.72
Displacement, resultant, in.	9.38	8.56	8.55	−8.74	−8.85
Displacement, z-direction, in.	1.40	1.27	1.28	−9.29	−8.57
Weight (lb)	25.56	27.68	28.07	8.31	9.75

TABLE 9.—COMPARISON OF TIP DISPLACEMENTS VALUES FOR INITIAL AND OPTIMUM DESIGNS

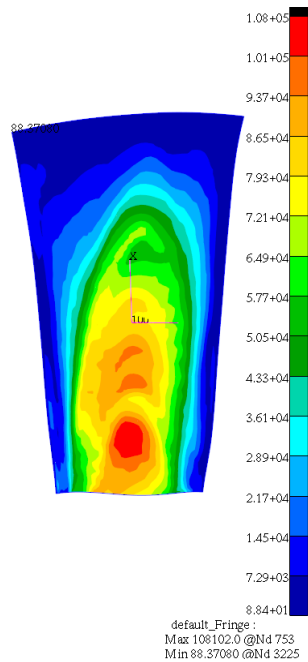
Constraint number: tip node	Initial	NEWSUMT optimum	NLPQ optimum	NEWSUMT percent difference	NLPQ percent difference	Remarks
16 : 3225	-0.374	-0.340	-0.341	-9.26	-8.84	
17 : 3276	0.549	0.500	0.500	-8.98	-8.98	Active

TABLE 10.—COMPARISON OF STRENGTH RATIO CONSTRAINT VALUES BETWEEN INITIAL AND OPTIMUM DESIGNS

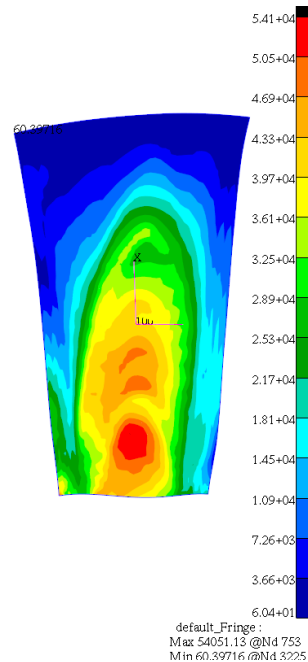
Constraint number	Initial strength ratio	NEWSUMT optimum strength ratio	NLPQ optimum strength ratio	NEWSUMT percent difference	NLPQ percent difference	Remarks
1	1.356	1.580	1.538	16.52	13.42	Active
2	1.681	1.853	1.894	10.23	12.67	
3	1.780	2.070	1.953	16.29	9.72	
4	1.874	2.293	2.091	22.36	11.58	
5	1.821	2.280	2.002	25.21	9.94	
6	1.857	2.029	1.982	9.26	6.73	
7	1.216	1.508	1.500	24.01	23.36	Active
8	1.422	1.788	1.666	25.74	17.16	
9	1.572	1.908	1.927	21.37	22.58	
10	1.629	1.772	1.869	8.78	14.73	
11	1.621	1.979	1.809	22.09	11.60	
12	1.766	1.731	1.745	-1.98	-1.19	
13	1.904	1.802	1.711	-5.36	-10.14	
14	2.169	1.931	2.314	-10.97	6.69	
15	2.400	1.973	2.157	-17.79	-10.13	

The optimum weight however, increased slightly. The increase in the optimum weight by both optimizers is due to constraint numbers 1, 7, and 8 which were initially violated with strength ratios of 1.356, 1.216, and 1.422 respectively, which are below the minimum allowable of 1.5 (Table 10). The optimization process made these constraints feasible and active by both optimization methods, as shown in Table 10. The optimized strength ratio value for constraint numbers 1, 7, and 8 became 1.580, 1.508, and 1.788 by NEWSUMT and 1.538, 1.5, and 1.666 by NLPQ optimizer. Constraint number 17, which is the radial displacement at tip node 3276, became active by both optimizers. (Active constraint is assumed to be within 0.02 percent of the lower and/or upper bound). Stress plots of these results are shown in Figure 27 and deformation plots in Figure 28.

Failure indices and strength ratio plots from the NEWSUMT optimum design are depicted in Figure 29. The optimum composite blade design does not exhibit any ply failures since the maximum failure index is 0.483 which is less than 1.0 and the minimum strength ratio over the 15 design groups is greater than 1.58 which takes into account the minimum safety factor of 1.5. Strength ratio of less than 1.0 exhibits ply failure.

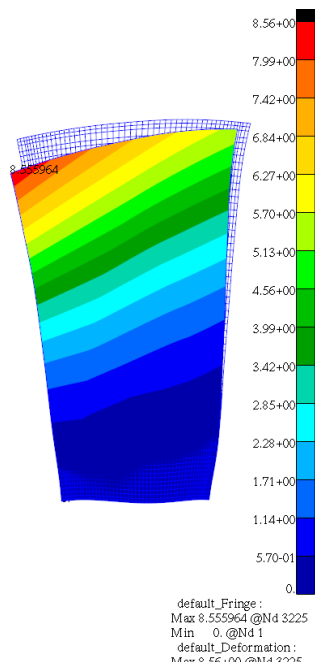


(a) Optimum design:  
Max Principal Stress = 108,102 psi

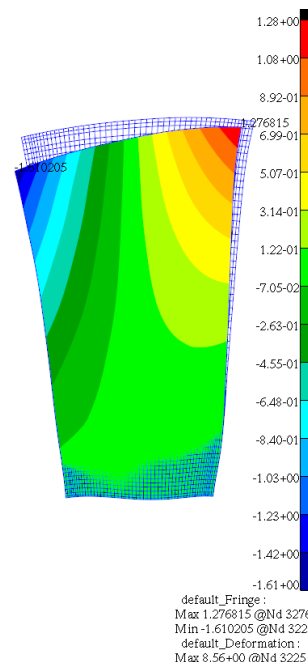


(b) Optimum design:  
Max Shear Stress = 54,051 psi

Figure 27.—Optimum design of the composite blade results (a) maximum principal stress, (b) maximum shear stress.



(a) Optimum design:  
Displacement Resultant = 8.56 in.



(b) Optimum design:  
Displacement z-direction = 1.27 in.

Figure 28.—Optimum design of the composite blade results (a) displacement resultant, (b) displacement in z-direction.

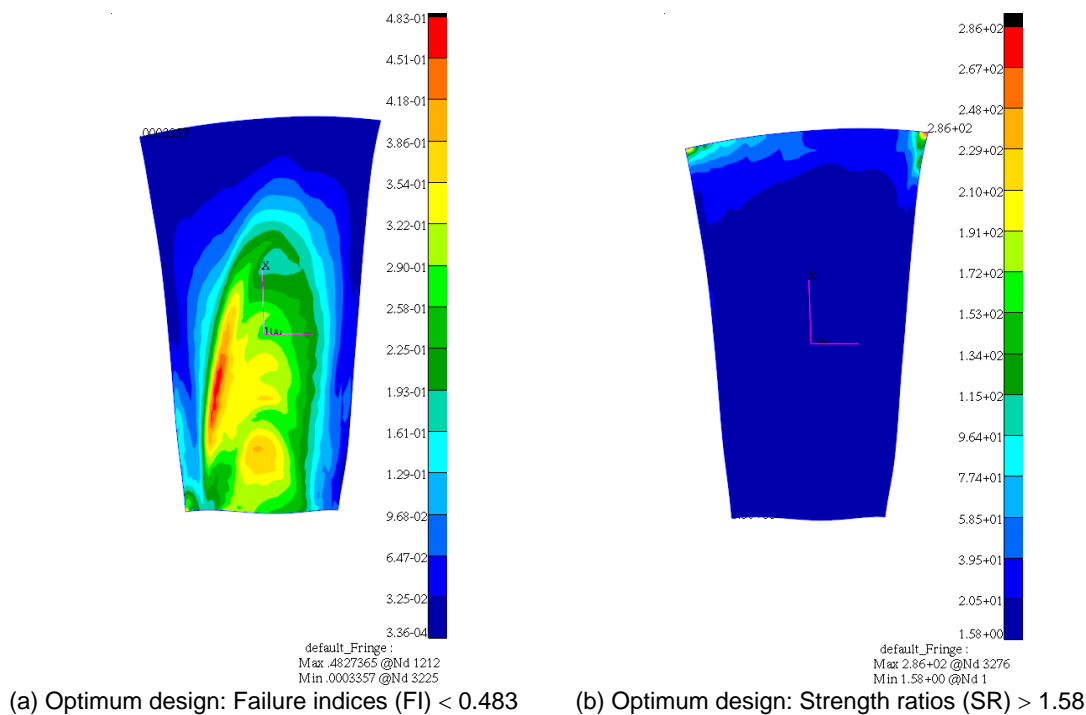


Figure 29.—Optimum design: (a) failure index, (b) strength ratio.

TABLE 11.—COMPARISON OF INITIAL AND OPTIMUM DESIGNS OF THE COMPOSITE BLADE

Design variable	Initial number of plies	Initial ply thickness	Initial core thickness	Total laminate thickness	NEWSUMT		NLPQ	
					Optimum ply thickness	Optimum core thickness	Optimum ply thickness	Optimum core thickness
1	4	0.025	0.000	0.1	0.025	0.000	0.025	0.000
2	8	0.025	0.000	0.2	0.025	0.000	0.025	0.000
3	12	0.025	0.000	0.3	0.025	0.000	0.025	0.000
4	16	0.025	0.000	0.4	0.025	0.000	0.025	0.000
5	20	0.025	0.000	0.5	0.025	0.000	0.025	0.000
6	24	0.025	0.000	0.6	0.025	0.000	0.025	0.000
7	8	0.025	0.500	0.7	0.033	0.434	0.038	0.395
8	12	0.025	0.500	0.8	0.034	0.388	0.032	0.415
9	16	0.025	0.500	0.9	0.033	0.374	0.035	0.345
10	20	0.025	0.500	1	0.029	0.424	0.032	0.358
11	24	0.025	0.500	1.1	0.045	0.015	0.030	0.386
12	28	0.025	0.500	1.2	0.024	0.529	0.024	0.534
13	32	0.025	0.500	1.3	0.022	0.601	0.021	0.617
14	36	0.025	0.500	1.4	0.019	0.711	0.038	0.015
15	40	0.025	0.500	1.5	0.017	0.826	0.021	0.664

The optimum design by both NEWSUMT and NLPQ optimization methods along with a comparison with the initial design of the composite blade, are shown in Table 11. For the first six design groups, ply thickness was passive in the optimization process (i.e., not allowed to vary). The honeycomb core thickness was updated for design variables 7 through 15 as shown in Table 11. The lower and upper bounds of the design variables were set at 0.001 and 1.0 in., respectively. For NEWSUMT the minimum core thickness varied between 0.015 in. for design group 11 and 0.826 in. for design group 15. The ply thickness in column 6 for NEWSUMT and column 8 for NLPQ both in Table 11 is calculated as follows:

Optimum ply thickness = (total laminate thickness – optimum core thickness)/initial number of plies

In the optimization results, the total laminate thickness for each design group remains at the same value as the initial laminate thickness thus maintaining the aerodynamic and geometric parameters and verified as follows:

Total laminate thickness = initial number of plies\*(optimum ply thickness) + optimum core thickness

## 5.2 Dynamic Analysis Results of the Optimized Composite Design

Dynamic analysis results of the optimized design of the composite blade were calculated using MSC/Nastran SOL 103 analysis solver (Ref. 2). Results of the first six natural modes from the MSC/Nastran dynamic calculations and comparison with the initial frequency of the composite design are summarized in Table 12. Similar to the initial composite design results, all six modes are evenly distributed in the frequency domain. Eigenvalue plots of the first six natural modes are depicted in Figure 30(a) to (c) and Figure 31(a) to (c). The modes depicted in the figures can be divided into bending modes (1<sup>st</sup>, 2<sup>nd</sup>, 4<sup>th</sup>, and 6<sup>th</sup> modes) and torsion modes (3<sup>rd</sup> and 5<sup>th</sup> modes).

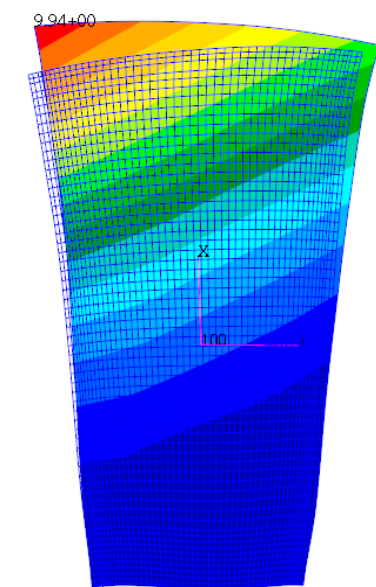
TABLE 12.—COMPARISON OF NATURAL FREQUENCIES (HZ) FOR THE INITIAL AND OPTIMIZED COMPOSITE DESIGN

Mode number	Initial frequency	Optimum frequency NEWSUMT	Optimum frequency NLPQ	Percent difference NEWSUMT	Percent difference NLPQ
Mode 1	19.472	19.915	19.773	2.28	1.55
Mode 2	58.792	63.075	60.745	7.29	3.32
Mode 3	110.320	115.372	114.745	4.58	4.01
Mode 4	150.936	158.179	153.801	4.80	1.90
Mode 5	248.470	251.893	251.541	1.38	1.24
Mode 6	263.912	268.871	270.126	1.88	2.35

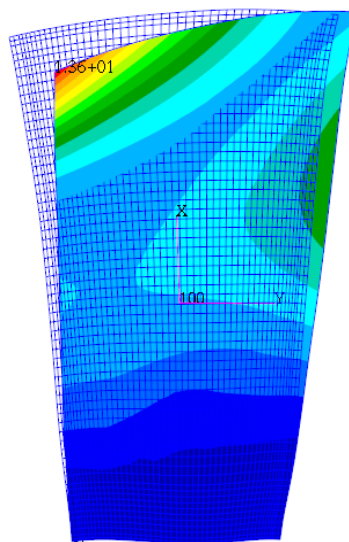
Default, Mode 1:Freq.=19.915, Eigenvectors, Translational

Default, Mode 2:Freq.=63.075, Eigenvectors, Translational

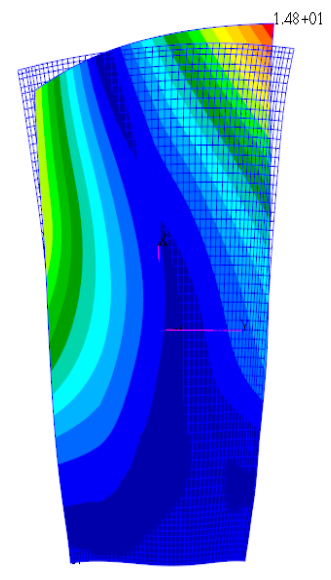
Default, Mode 3:Freq.=115.37, Eigenvectors, Translational



(a) Optimum design  
Mode 1: Frequency = 19.915 Hz



(b) Optimum design  
Mode 2: Frequency = 63.075 Hz



(c) Optimum design  
Mode 3: Frequency = 115.37 Hz

Figure 30.—Mode shapes for the optimum design of the composite blade (a) mode 1, (b) mode 2, (c) mode 3.

Default, Mode 4:Freq.=158.18, Eigenvectors, Translationa ; Default, Mode 5:Freq.=251.89, Eigenvectors, Translat ; Default, Mode 6:Freq.=268.87, Eigenvectors, Translat

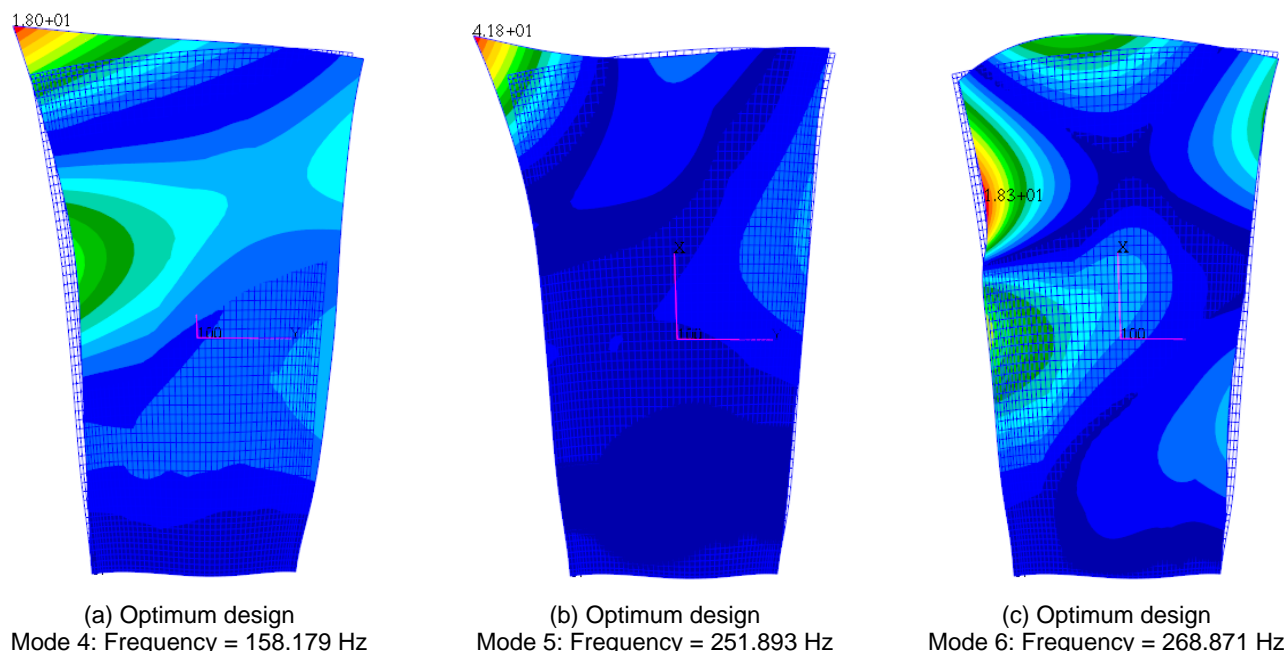


Figure 31.—Mode shapes for the optimum design of the composite blade (a) mode 4, (b) mode 5, (c) mode 6.

## 6.0 Discrete Optimization to Obtain Number of Plies

Discrete optimization is performed to obtain the optimum number of plies. Once the optimum design is obtained from the optimizer, discrete optimization and final static analysis is performed to obtain the minimum number of plies and the optimum weight. Table 13 depicts the number of plies back-calculated from the NEWSUMT optimum design. Design variables (1 to 6) remain passive. The calculation is approximated by rounding up the real numbers to integers as shown in Column 4 of Table 13. The ply lay-up is adjusted to fit the specified ply lay-up, which is in increments of 4 plies, as shown earlier for the symmetric lay-up specification in Table 5. The core thickness of the blade (last column in Table 13) and the optimum number of plies (3<sup>rd</sup> column in Table 13) are back-calculated as follows:

$$\text{Core thickness} = \text{Total laminate thickness} - (\text{optimum number of plies} \times 0.025)$$

Optimum number of plies = (Optimum ply thickness) \* (Initial number of plies) / 0.025, where 0.025 is the assumed initial ply thickness.

The number of plies for NLPQ is back-calculated following the same process as NEWSUMT. Results at the final iteration are considered for this method since convergence was not fully achieved. The number of plies back-calculated from the NLPQ last iteration, considered as optimum, are given in Table 14. The core thickness and optimum number of plies are calculated as presented above for the NEWSUMT design.



TABLE 13.—NUMBER OF PLYS BACK-CALCULATED FROM NEWSUMT OPTIMUM DESIGN

Design variable	Initial number of plies	Optimum number of plies	Round optimum number of plies	Adjust for symmetric ply lay-up	Updated half core thickness (symmetric)
1	4	4	4	2	0
2	8	8	8	4	0
3	12	12	12	6	0
4	16	16	16	8	0
5	20	20	20	10	0
6	24	24	24	12	0
7	8	10.624	11	6	0.200
8	12	16.478	16	8	0.200
9	16	21.041	21	10	0.200
10	20	23.049	23	12	0.200
11	24	43.397	43	22	0.000
12	28	26.829	27	14	0.250
13	32	27.976	28	14	0.300
14	36	27.560	28	14	0.350
15	40	26.940	27	14	0.400

TABLE 14.—NUMBER OF PLYS BACK-CALCULATED FROM NLPQ OPTIMUM DESIGN

Design variable	Initial number of plies	Optimum number of plies	Round optimum number of plies	Adjust for symmetric ply lay-up	Updated half core thickness (symmetric)
1	4	4	4	2	0
2	8	8	8	4	0
3	12	12	12	6	0
4	16	16	16	8	0
5	20	20	20	10	0
6	24	24	24	12	0
7	8	10.624	11	6	0.200
8	12	16.478	16	8	0.200
9	16	21.041	21	10	0.200
10	20	23.049	23	12	0.200
11	24	43.397	43	22	0.000
12	28	26.829	27	14	0.250
13	32	27.976	28	14	0.300
14	36	27.560	28	14	0.350
15	40	26.940	27	14	0.400

## 7.0 Final Analysis Results and Discussion of the Optimized Composite Blade

Final static and dynamic analyses is required in the final step of the sandwich composite blade design process to calculate/verify the final weight, ply strength ratios, deformations and mode shapes using the optimum ply lay-up sequence, number of plies and corresponding core thicknesses.

In this final step, MSC/Nastran database PCOMP entries are updated with the new number of plies and core thickness and final static (SOL 101) and dynamic (SOL 103) analyses are executed. The integer number of plies and core thickness from the NEWSUMT design, as given in Table 13 columns 5 and 6, and the design obtained from NLPQ optimizer, as given in Table 14, columns 5 and 6, were considered for the final analysis of the sandwich composite blade, in two separate runs.

The initial ply thickness for the all design variables remained fixed at 0.025 in. The core thicknesses of design variables 7 to 15 and the number of plies for these variables, as given in the last column of Tables 13 and 14 were entered in the PCOMP cards in the MSC/Nastran database for each of the runs. The final number of plies and core thicknesses for each design variable group is shown in Table 15. From Table 15 we observe the following:

- For design variable 7, the number of plies was increased to 12 from 8 for both NEWSUMT and NLPQ optimizers and the core thickness was reduced from the initial 0.5 to 0.4 in.
- For design variable 8, the number of plies was increased to 16 from 12 with both optimizers while the core thickness was reduced from the initial 0.5 to 0.4 in.
- For design variable 9, the number of plies was increased to 20 from 16 with both optimizers while the core thickness was reduced from the initial 0.5 to 0.4 in.
- For design variable 10, the number of plies was increased to 24 from 20 with both optimizers while the core thickness was reduced from the initial 0.5 to 0.4 in.
- For design variable 11, the number of plies was increased to 44 from 24 with NEWSUMT optimization process while the core thickness was reduced from the initial 0.5 to 0.0 in. Therefore, no core thickness is required in the final analysis run for design variable 11 but the number of plies was increased from 24 to 44. With the NLPQ optimum design the number of plies was increased to 28 from the initial 24 and the core thickness was reduced to 0.4 from the initial 0.5 in.
- For design variable 12, the number of plies and core thickness remained unchanged at 28 plies with core thickness of 0.5 in. for both optimizers.
- For design variable 13, the number of plies was reduced to 28 from 32 while the core thickness increased to 0.6 in. from the initial 0.5 in., with both optimizers.
- For design variable 14, the number of plies was reduced to 28 from 36 with NEWSUMT optimizer with increased core thickness to 0.7 in. from the initial 0.5 in. With the NLPQ optimum design the number of plies were increased to 56 and no core ply.
- For design variable 15, the number of plies was reduced to 28 from 40 with NEWSUMT optimizer while the core thickness increased to 0.8 in. from the initial 0.5 in. For NLPQ the number of plies was reduced to 32 with an increase in the core thickness to 0.7 in.

TABLE 15.—FINAL NUMBER OF PLIES AND CORE THICKNESSES COMPARED WITH INITIAL DESIGN

Design variable:	Initial		NEWSUMT design		NLPQ design	
	Number of plies	Core thickness	Number of plies	Core thickness	Number of plies	Core thickness
1	4	0.0	4	0.0	4	0.0
2	8	0.0	8	0.0	8	0.0
3	12	0.0	12	0.0	12	0.0
4	16	0.0	16	0.0	16	0.0
5	20	0.0	20	0.0	20	0.0
6	24	0.0	24	0.0	24	0.0
7	8	0.5	12	0.4	12	0.4
8	12	0.5	16	0.4	16	0.4
9	16	0.5	20	0.4	20	0.4
10	20	0.5	24	0.4	24	0.4
11	24	0.5	44	0.0	28	0.4
12	28	0.5	28	0.5	28	0.5
13	32	0.5	28	0.6	28	0.6
14	36	0.5	28	0.7	56	0.0
15	40	0.5	28	0.8	32	0.7

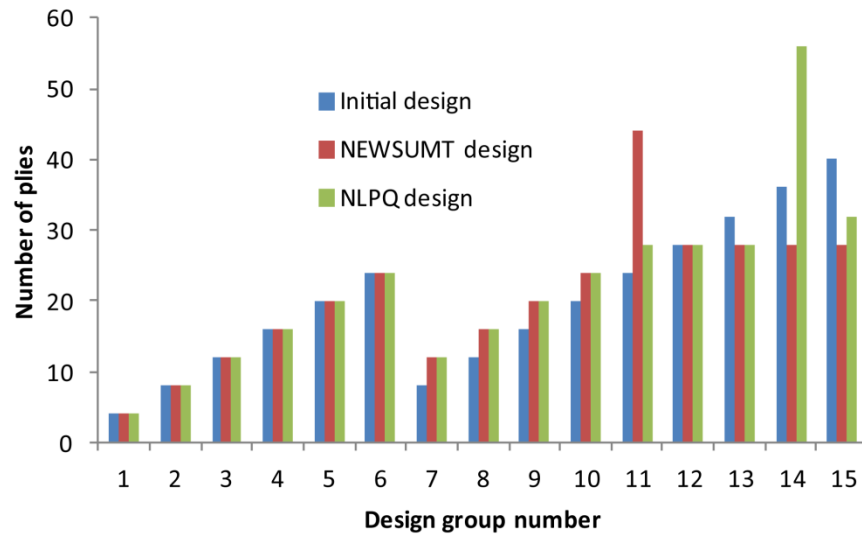


Figure 32.—Number of plies in final analysis for each design group (excluding core ply).

The number of plies in the final analysis for each design group and comparison with the initial design is plotted in Figure 32.

The final symmetric ply lay-up with the NEWSUMT optimizer for each design group, denoted with an (F), is shown in Table 16 along with comparison with the initial ply lay-up (I). Ply symmetry is denoted with a subscript ([ ]<sub>s</sub>). In final analysis, for design group 7, four additional plies were required, shown as 90/0 in red, considering symmetry (Table 16). Similarly, for design groups 8, 9 and 10, four additional plies were required in final analysis. Design group 11 required 20 additional plies with no core ply. The lay-up sequence for the additional plies that produced the best design for this design group was the [90/0/0/0/0/0/0/0/0] degree angles. This is because at [90/45/−45] degree angles, the ply stiffness and strength are much more like the matrix properties than the fiber properties, whereas, at 0° in the fiber direction, the properties are fiber dominated (Ref. 8). The number of ply shapes or designs was reduced to 8 in the final analysis from the initial 10, as shown in the last row of Table 16. A comparison of the initial and final ply lay-up shapes is provided in the next section.

## 7.1 Comparison of Initial and Final Ply Build-Up Shapes

The blade was designed initially with 10 ply lay-up shapes, as shown in Figures 17 to 19. The final optimization process with the NEWSUMT optimum design reduced the 10 ply lay-up shapes to 8, as shown in Table 16 and Figures 33 to 38. A side-by-side comparison of the initial ply shape and final ply shape, shown in these figures as follows:

- The optimum design of ply shape 3, includes the four additional plies in design group 7, as shown in Figure 33.
- The optimum ply shape 4 includes the four additional plies for design group 8, shown in Figure 34.
- Optimum ply shape 5 includes the four additional plies for design group 9, shown in Figure 35.
- Optimum ply shape 6 includes the four additional plies for design group 10, shown in Figure 36.
- Optimum ply shape 7 includes ten additional plies for design group 11, shown in Figure 37.
- New ply shape 8 includes the eight-zero degree angles [0/0/0/0/0/0/0/0] for design group 11, shown in Figure 38.

The initial ply shape layups (8, 9, and 10) of design groups (13, 14, and 15) were eliminated from the final optimization, as shown crossed off in red in Table 16.

TABLE 16.—FINAL ANALYSIS (F) SYMMETRIC PLY LAYUP FROM NEWSUMT DESIGN, AND COMPARISON WITH INITIAL (I), CORE PLY DENOTED WITH AN ASTERISK\*

Group number	Optimum Ply Layup with NEWSUMT Optimizer
1 (I)	[0/90] <sub>s</sub>
1 (F)	[0/90] <sub>s</sub>
2 (I)	[0/90/45/-45] <sub>s</sub>
2 (F)	[0/90/45/-45] <sub>s</sub>
3 (I)	[0/90/45/-45/90/0] <sub>s</sub>
3 (F)	[0/90/45/-45/90/0] <sub>s</sub>
4 (I)	[0/90/45/-45/90/0/-45/45] <sub>s</sub>
4 (F)	[0/90/45/-45/90/0/-45/45] <sub>s</sub>
5 (I)	[0/90/45/-45/90/0/-45/45/0/90] <sub>s</sub>
5 (F)	[0/90/45/-45/90/0/-45/45/0/90] <sub>s</sub>
6 (I)	[0/90/45/-45/90/0/-45/45/0/90/45/-45] <sub>s</sub>
6 (F)	[0/90/45/-45/90/0/-45/45/0/90/45/-45] <sub>s</sub>
7 (I)	[0/90/45/-45/*] <sub>s</sub>
7 (F)	[0/90/45/-45/90/0/*] <sub>s</sub>
8 (I)	[0/90/45/-45/90/0/*] <sub>s</sub>
8 (F)	[0/90/45/-45/90/0/-45/45/*] <sub>s</sub>
9 (I)	[0/90/45/-45/90/0/-45/45/*] <sub>s</sub>
9 (F)	[0/90/45/-45/90/0/-45/45/0/90/*] <sub>s</sub>
10 (I)	[0/90/45/-45/90/0/-45/45/0/90/*] <sub>s</sub>
10 (F)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/*] <sub>s</sub>
11 (I)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/*] <sub>s</sub>
11 (F)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/0/0/0/0/0/*] <sub>s</sub>
12 (I)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/*] <sub>s</sub>
12 (F)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/*] <sub>s</sub>
13 (I)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/-45/45/*] <sub>s</sub>
13 (F)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/*] <sub>s</sub>
14 (I)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/-45/45/0/90/*] <sub>s</sub>
14 (F)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/*] <sub>s</sub>
15 (I)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/-45/45/0/90/45/-45/*] <sub>s</sub>
15 (F)	[0/90/45/-45/90/0/-45/45/0/90/45/-45/90/0/*] <sub>s</sub>
Ply shapes:	1      2      3      4      5      6      7      8 (0° plies)

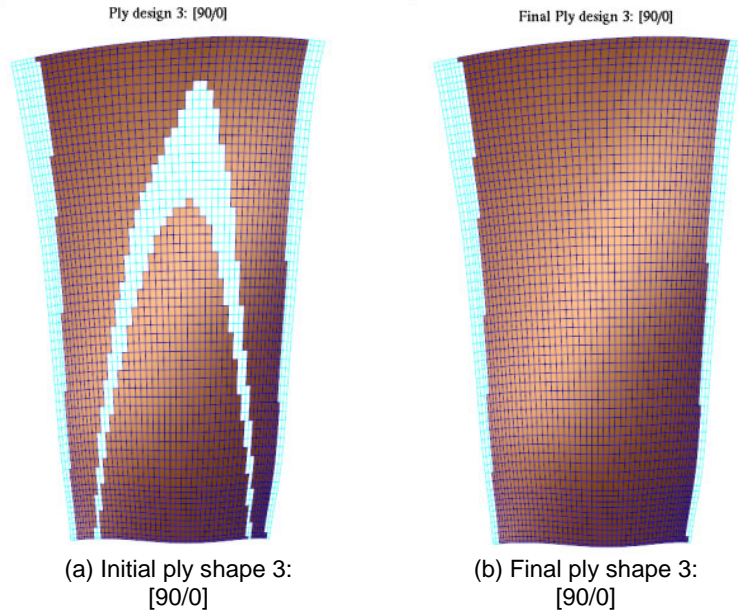


Figure 33.—Comparison of ply shapes: (a) initial ply shape 3, (b) final ply shape 3.

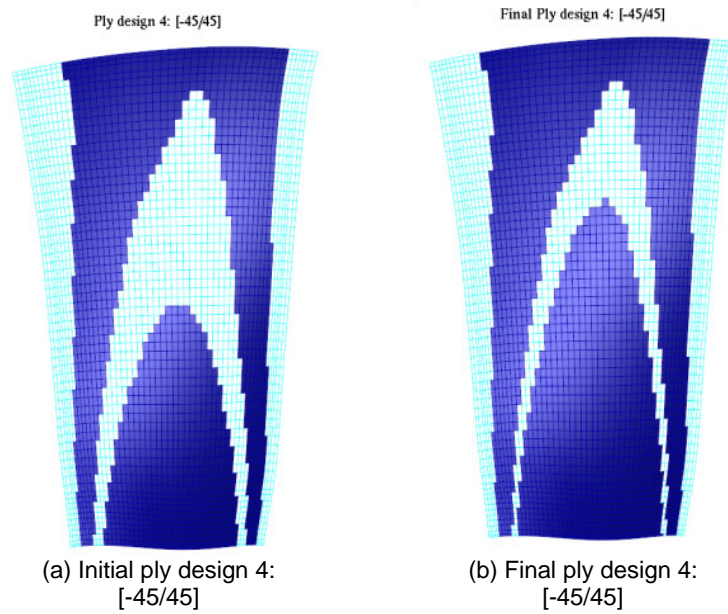


Figure 34.—Comparison of ply shapes: (a) initial ply shape 4, (b) final ply shape 4.

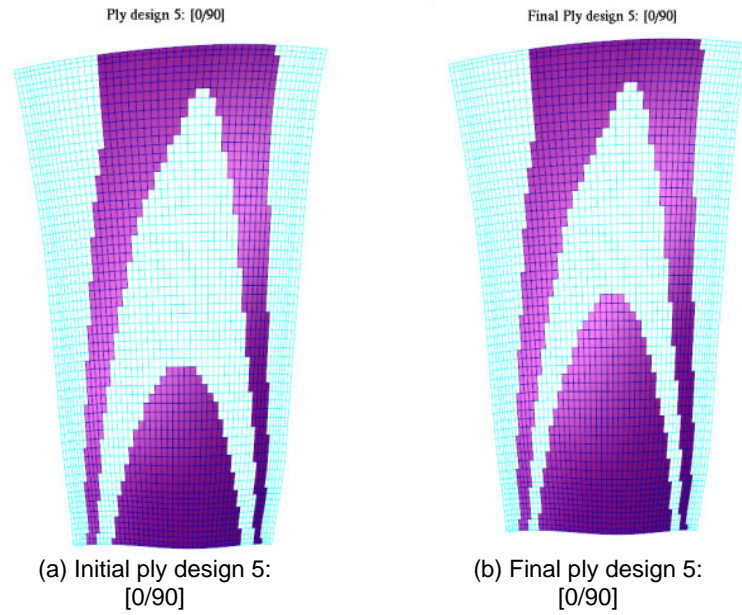


Figure 35.—Comparison of ply shapes: (a) initial ply shape 5, (b) final ply shape 5.

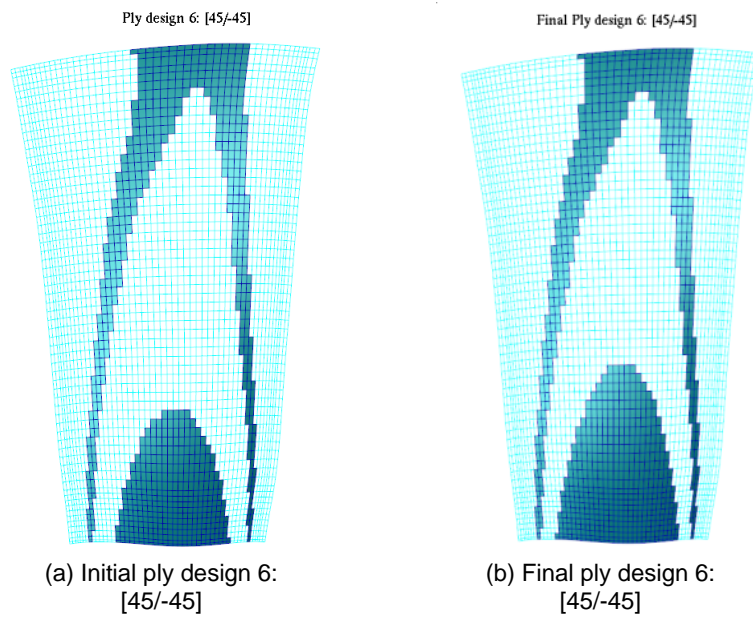


Figure 36.—Comparison of ply shapes: (a) initial ply shape 6, (b) final ply shape 6.

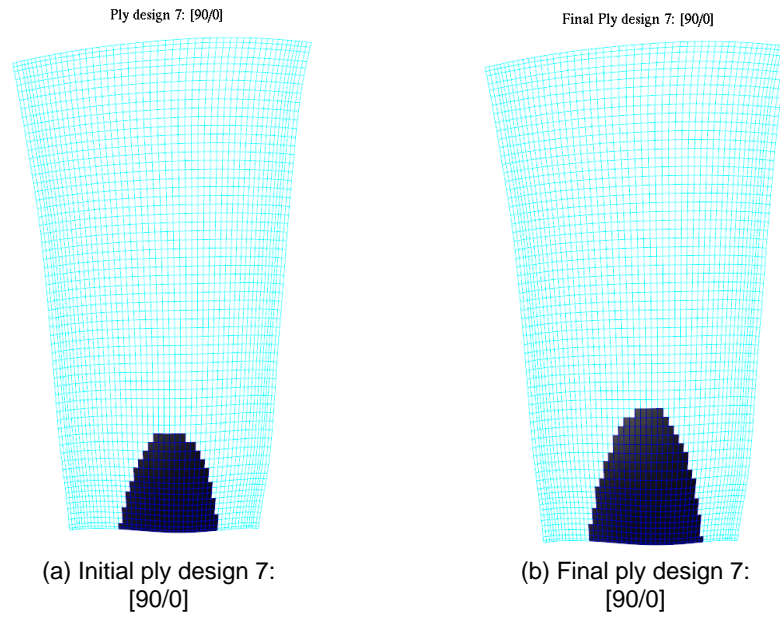


Figure 37.—Comparison of ply shapes: (a) initial ply shape 7, (b) final ply shape 7.

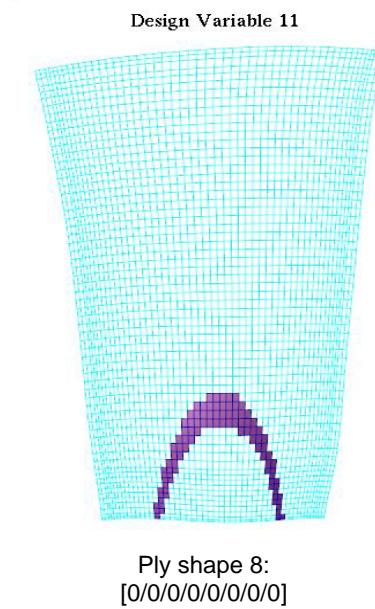


Figure 38.—New ply shape 8.

## 7.2 Final Static Analysis Results

A final static analysis was executed of the updated MSC/Nastran database and the results are shown in Table 18. Comparing with the initial design the final weight was increased from 25.56 to 27.94 lb with NEWSUMT and to 27.84 lb with NLPQ. The initial design was not feasible because at least one strength ratio constraint did not meet the design criteria, as shown in Table 10. The maximum principal stress and maximum shear stress results with percent differences are given in Table 17. Both maximum principal stress and max shear stresses were reduced in the final analysis by both NEWSUMT and NLPQ optimum designs. The percent difference for NEWSUMT was 8 percent for maximum principal stress and 9.22 percent for maximum shear stress. The differences for NLPQ were 9.78 percent reduction and 10.98 percent for maximum principal stress and maximum shear stress, respectively. The displacement magnitude was reduced in the final analysis, 10.55 percent by the NEWSUMT design and 8.57 percent by the NLPQ design. The final stress and deformation plots are depicted in Figures 39 and 40.

Radial tip displacements were also reduced by both optimizers at tip nodes 3225 and 3276, as shown in Table 18. The percent reduction was 10.5 percent with NEWSUMT for both tip nodes and about 9 percent with NLPQ.

Final analysis results of strength ratio and comparison with the initial ratios is shown in Table 19. Percent difference with NEWSUMT ranged from 2.6 percent reduction to 43.2 percent increase. The final analysis from the NEWSUMT optimum design shows all strength ratio values to be in the feasible domain, i.e., greater than or equal to 1.5 and less than, or equal to 3.0, which account for the safety factor. The final analysis using the NLPQ optimum design however produced a slightly infeasible constraint, namely constraint number 7. The strength ratio for constraint number 7, as shown in Table 19, was 1.387 for NLPQ which is less than the allowable of 1.5 but since the ratio is greater than 1.0, it passes the ply failure TSAI-WU test criteria. This non feasibility is because NLPQ failed to converge at the maximum allowable iterations.

Final analysis results for failure indices and strength ratio from both NEWSUMT and NLPQ optimum designs are depicted in Figure 41. The final sandwich composite blade analysis does not exhibit any ply failures since the maximum failure index is 0.479, which is less than 1.0, and the minimum strength ratio over all 15 design groups is greater than 1.60 which takes into account the minimum safety factor of 1.5.

TABLE 17.—FINAL ANALYSIS STATIC ANALYSIS RESULTS AND COMPARISON WITH INITIAL DESIGN

	Initial analysis	Final analysis NEWSUMT	Final analysis NLPQ	Percent difference NEWSUMT	Percent difference NLPQ
Max principal stress, psi	117,943	108,510.9	106,406.4	-8.00	-9.78
Max shear stress, psi	59,768.47	54,255.52	53,205.51	-9.22	-10.98
Displacement, resultant, in.	9.38	8.39	8.51	-10.55	-9.28
Displacement, z-direction, in.	1.4	1.26	1.28	-10.00	-8.57
Weight (lb)	25.56	27.94	27.84	9.33	8.93

TABLE 18.—FINAL ANALYSIS RESULTS OF RADIAL DISPLACEMENTS  
VALUES AND COMPARISON WITH INITIAL

Constraint number: tip node	Initial	Final analysis NEWSUMT	Final analysis NLPQ	Percent difference NEWSUMT	Percent difference NLPQ
16 : 3225	-0.374	-0.334	-0.341	-10.569	-8.97
17 : 3276	0.549	0.491	0.498	-10.589	-9.30



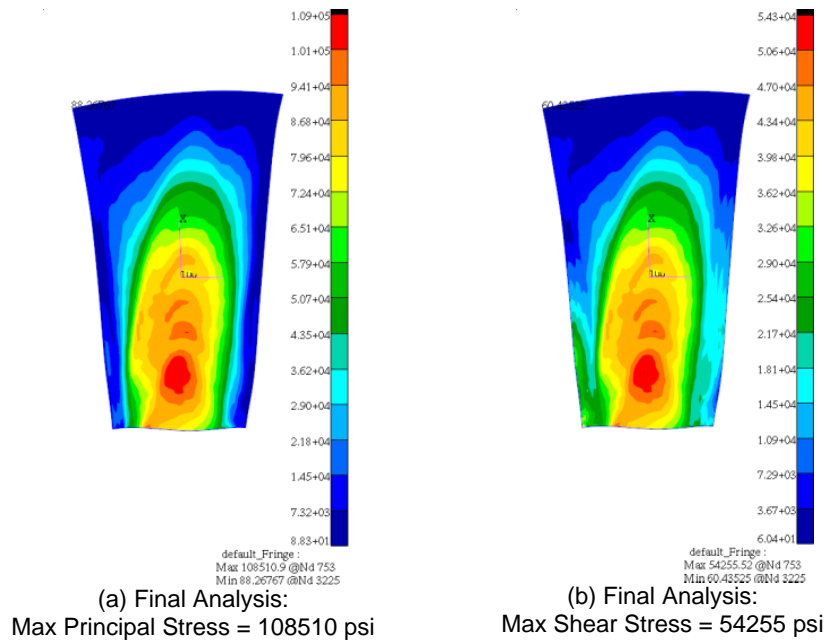


Figure 39.—Final analysis of the composite blade results (a) Maximum principal stress, (b) maximum shear stress.

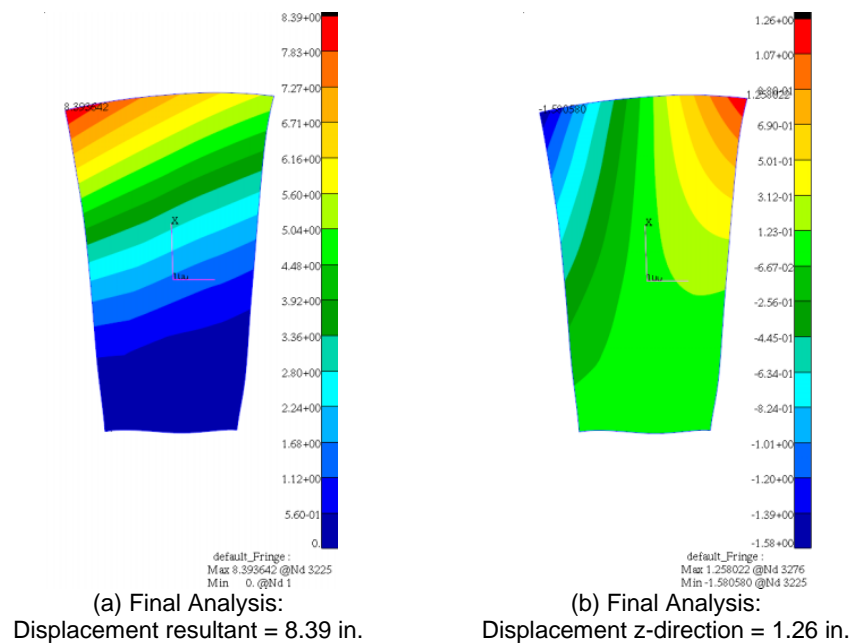


Figure 40.—Final analysis of the composite blade results (a) Displacement resultant, (b) displacement in z-direction.

TABLE 19.—FINAL ANALYSIS RESULTS OF STRENGTH RATIO  
VALUES AND COMPARISON WITH INITIAL

Constraint number	Initial strength ratio	Final analysis NEWSUMT	Final analysis NLPQ	Percent difference NEWSUMT	Percent difference NLPQ
1	1.356	1.943	1.589	43.257	17.17
2	1.681	2.192	1.952	30.414	16.11
3	1.780	2.386	2.011	34.062	12.98
4	1.874	2.630	2.153	40.363	14.87
5	1.821	2.816	2.055	54.662	12.83
6	1.857	2.071	1.959	11.522	5.51
7	1.216	1.528	1.387	25.676	14.08
8	1.422	1.947	1.845	36.898	29.78
9	1.572	1.902	1.814	21.004	15.37
10	1.629	1.760	1.732	8.025	6.33
11	1.621	1.504	1.821	-7.242	12.32
12	1.766	1.720	1.792	-2.607	1.47
13	1.904	1.819	1.829	-4.468	-3.94
14	2.169	1.950	2.141	-10.090	-1.30
15	2.400	2.073	2.069	-13.623	-13.80

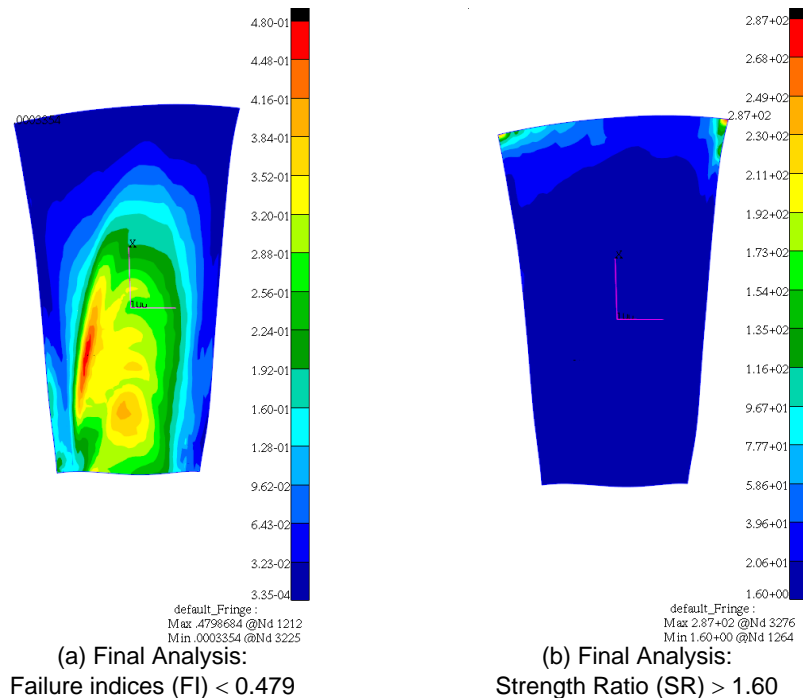


Figure 41.—Final analysis: (a) Failure index and (b) strength ratio.

### 7.3 Final Dynamic Analysis Results

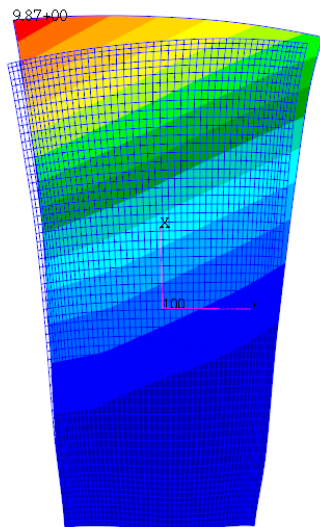
Dynamic analysis results of the final design of the sandwich composite blade were calculated using MSC/Nastran SOL 103 analysis solver. Results for the first six natural modes from the MSC/Nastran dynamic calculations and comparison with the initial frequency of the composite design are summarized in Table 20. Both optimizers produced slightly higher frequencies than the initial design, but this is expected since there was a small increase in the final weight.

Eigenvalue plots of the first six natural modes are depicted in Figures 42 and 43. As with the earlier mode shapes modes (1<sup>st</sup>, 2<sup>nd</sup>, 4<sup>th</sup>, and 6<sup>th</sup> modes) are bending modes and modes (3<sup>rd</sup> and 5<sup>th</sup>) are torsion modes.

TABLE 20.—COMPARISON OF NATURAL FREQUENCIES (HZ) FOR THE INITIAL AND THE FINAL COMPOSITE BLADE

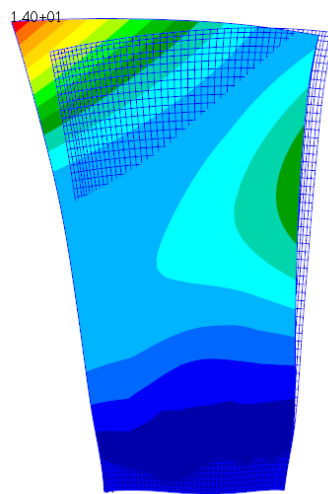
Mode number	Initial frequency	Final analysis NEWSUMT	Final analysis NLPQ	Percent difference NEWSUMT	Percent difference NLPQ
Mode 1	19.472	20.034	19.811	2.89	1.74
Mode 2	58.792	65.086	61.277	10.71	4.23
Mode 3	110.320	116.106	114.538	5.24	3.82
Mode 4	150.936	164.183	155.518	8.78	3.04
Mode 5	248.470	254.159	251.691	2.29	1.30
Mode 6	263.912	273.790	271.258	3.74	2.78

Default, Mode 1:Freq.=20.034, Eigenvectors, Translational



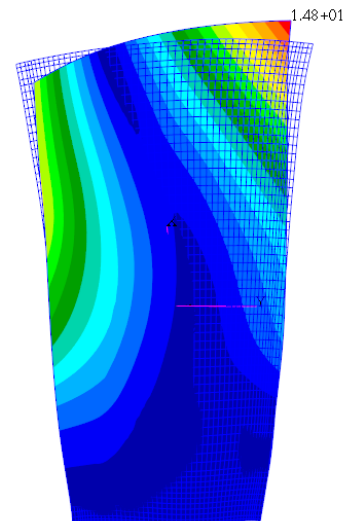
(a) Final Analysis  
Mode 1: Frequency = 20.034 Hz

Default, Mode 2:Freq.=65.086, Eigenvectors, Translational



(b) Final Analysis  
Mode 2: Frequency = 65.086 Hz

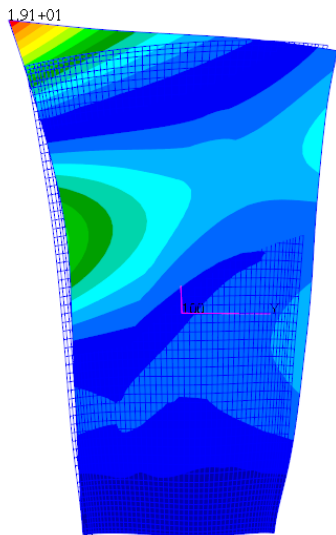
Default, Mode 3:Freq.=116.11, Eigenvectors, Translational



(c) Final Analysis  
Mode 3: Frequency = 116.11 Hz

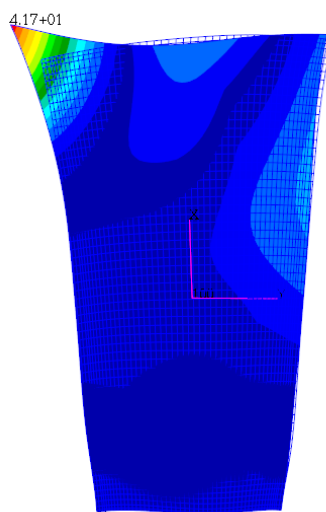
Figure 42.—Mode shapes for the final analysis of the composite blade (a) mode 1, (b) mode 2, (c) mode 3.

Default, Mode 4:Freq.=164.18, Eigenvectors, Translational



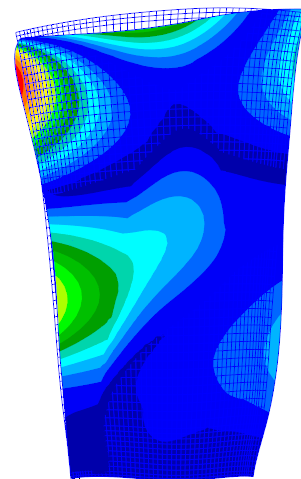
(a) Final Analysis  
Mode 4: Frequency = 164.18 Hz

Default, Mode 5:Freq.=254.16, Eigenvectors, Translational



(b) Final Analysis  
Mode 5: Frequency = 254.16 Hz

Default, Mode 6:Freq.=273.79, Eigenvectors, Translational



(c) Final Analysis  
Mode 6: Frequency = 273.79 Hz

Figure 43.—Mode shapes for the final analysis of the composite blade (a) mode 4, (b) mode 5, (c) mode 6.

## 8.0 Conclusions

An optimized design for a turbofan engine blade sized for a large aircraft engine was developed from a given baseline solid metallic model to a sandwich composite fan blade. The optimized composite blade design meets the aerodynamic and geometric considerations throughout the design process while the solution ensured that the final design was efficient and conformed to constraints imposed on radial displacement limitations and ply failure. The result was a lighter blade design, with mass savings of 72 percent compared to the metallic blade, when the combined pressure and centrifugal loads were considered. The maximum stresses and radial displacement for the final optimized composite blade were at much higher values than the metallic blade but still within their allowable limits. It was shown that the deformation behavior can be greatly influenced by the fiber orientation. It was also shown that the final design did not exhibit any ply failures considering an additional safety factor of 1.5 in the design process. Analyses and optimization was performed utilizing the OpenMDAO Framework, developed at NASA Glenn Research Center, which allows flexibility in case any modifications are required. The study performed in this paper highlights the continuing development of an optimization process for composite material lay-ups. Further research and development will continue, considering the application of an Integer programming algorithm to further refine the optimization process. Ply angle orientation may be optimized in addition to, or instead of, ply thickness depending on manufacturing considerations.

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14. ABSTRACT This report addresses the structural analysis and optimization of a composite fan blade sized for a large aircraft engine. An existing baseline solid metallic fan blade was used as a starting point to develop a hybrid honeycomb sandwich construction with a polymer matrix composite face sheet and honeycomb aluminum core replacing the original baseline solid metallic fan model made of titanium. The focus of this work is to design the sandwich composite blade with the optimum number of plies for the face sheet that will withstand the combined pressure and centrifugal loads while the constraints are satisfied and the baseline aerodynamic and geometric parameters are maintained. To satisfy the requirements, a sandwich construction for the blade is proposed with composite face sheets and a weak core made of honeycomb aluminum material. For aerodynamic considerations, the thickness of the core is optimized whereas the overall blade thickness is held fixed so as to not alter the original airfoil geometry. Weight is taken as the objective function to be minimized by varying the core thickness of the blade within specified upper and lower bounds. Constraints are imposed on radial displacement limitations and ply failure strength. From the optimum design, the minimum number of plies, which will not fail, is back-calculated. The ply lay-up of the blade is adjusted from the calculated number of plies and final structural analysis is performed. Analyses were carried out by utilizing the OpenMDAO Framework, developed at NASA Glenn Research Center combining optimization with structural assessment.					
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